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Coordinate Conversion Technique for OTH  
Backscatter Radar,

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TERENCE J. ELKINS  
JOSEPH GIBBS

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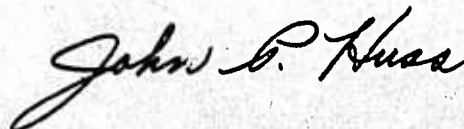
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A radio propagation simulation computer program, known as WIMP (World-Wide Ionospheric Modelling Program), has been studied and documented. The purpose of the program is to permit the transformation from Over-The-Horizon (OTH) Backscatter radar coordinates to geographic coordinates, given a vertical incidence and a backscatter ionogram measured at the radar site. The program consists of a three-dimensional ionospheric modelling algorithm, which contains a provision for updating on the basis of the ionograms, followed by a ray-tracing procedure. These algorithms have		

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been deduced from a program source deck and the program structure has been documented in terms of mathematical algorithms and flow charts, together with program listings.

The algorithms have been compared with others in use at RADC and quantitative results of this comparison are presented. These consist of ionospheric model comparisons for representative ranges of the model parameters. Finally, a measured backscatter ionogram is simulated, using the RADC program, and the ionospheric structure along the sounder boresight is deduced.

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## Coordinate Conversion Technique for OTH Backscatter Radar

### 1. INTRODUCTION

The WIMP Program is a complex algorithm which purports to permit accurate conversion from radar target range coordinates to geographic target coordinates in OTH Backscatter HF radar applications; the complexity is fundamentally due to a deeply developed iterative and reiterative algorithm that ultimately involves the user. The program consists of three main components:

- (a) A set of subprograms which construct a three-dimensional three-layer ionospheric model.
- (b) A set of subprograms which simulate HF radio wave propagation in the ionosphere constructed in (a).
- (c) One of three driving programs controlling the calling sequence to the radio wave propagation simulator in (b); these driving programs perform the following tasks: (1) From a given ionosphere, generate the leading edge of a simulated oblique ionogram including scale factors to the  $F_2$ -layer parameters to force agreement with a given vertical ionogram; (2) from a comparison of the simulation in (1) to a given oblique ionogram generate range gradient factors to apply to  $f_o F_2$  and  $M(3000)F_2$  to force agreement; (3) from the final ionosphere generated in (1) and (2), simulate predicted radio frequency propagation paths, from which range vs group path functions may be tabulated.

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We first describe in some detail the WIMP three-dimensional three-layer ionospheric model, followed by a general description of the radio wave propagation simulation subprogram (ray-tracing algorithm). A functional description is given of the three driving programs; the operating instructions for their use are included next.

Program block diagrams, flow charts, and program listings are included in Appendixes A, B, and C.

Comparisons have been made of the results of the WIMP ray tracings with techniques developed at RADC. The description and results of these studies are reported in Sections 19 through 21.

## 2. THE WIMP 3-D IONOSPHERIC MODEL

A complete three-dimensional ionospheric model generally consists of three fundamental aspects: (1) How many distinct layers are to be included, (2) How shall the layer parameters be modelled, (3) How shall the electron density profile be erected from the modelled parameters? A collateral question, equally important is, what ray-tracing technique is to be used, that is, which aspect dominates the simulation of HF propagation? To put the following discussion in proper perspective the latter question will be considered here in general, reserving a more detailed treatment to a latter section.

The WIMP ray-tracing algorithm, SUBROUTINE TRISL, is a control point technique based on layer parameters as in the ITS-78 program<sup>1</sup> and the DEVAN program.<sup>2,3</sup> The treatment of gradients of electron density, however, differs: ITS-78 does not consider gradients explicitly, DEVAN constructs an equivalent tilted reflecting surface from variations in virtual height, while WIMP constructs the tilt of the reflecting layer from the gradients of electron density. The predictions of the WIMP model are primarily sensitive to the layer parameter predictions, and only weakly sensitive to the electron density profile model. This latter dependence only enters the calculation at the reflection point (which generally is within the  $F_2$  layer), and involves the horizontal gradients of the electron density which are determined primarily by the gradients of the  $F_2$ -layer parameters.

The WIMP model ray tracing considers three distinct layers, E,  $F_1$ , and  $F_2$ ; an optional D-layer tail may be appended to the E layer. The E-layer critical

1. Barghausen, A. F., et al (1969) Predicting Long-Term Operational Parameters of High-Frequency Sky-Wave Telecommunication Systems, ESSA Technical Report ERL 110-ITS-78, Institute for Telecommunication Sciences, Boulder, CO.
2. Beckwith, R. I., Bailey, A. D., and Rao, N. N. (1972) An Investigation of Directional Propagation Effects in High-Frequency Radio Source Location, RRL Publication No. 409.
3. Beckwith, R. I. (1973) A Computer Program for the Rapid Prediction of Angles of Arrival of HF Radio Waves, RRL Publication No. 442.

frequency is determined from the local solar zenith angle. The model employed for the latter is sufficiently unique to describe in some detail below. The  $F_1$  critical frequency is 25 percent larger than  $f_o E$  with an additional 0.5 MHz.

The ITS model provides predictions for the  $F_2$  critical frequency and  $M(3000)$  factor. These parameters may be modified by ad hoc scale factors to force agreement with a given vertical ionogram, and ad hoc gradient factors to force agreement with a given oblique ionogram. The  $F_2$  semithickness is determined from a linear sunspot model. All parameters thus far mentioned are used to generate the  $F_2$ -layer height.

The  $F_1$  layer is fitted between the E and  $F_2$  layers such that the  $F_1$  bottom coincides with the E-layer height and the  $F_1$ -layer height coincides with the  $F_2$ -layer bottom.

A more detailed description of the layer parameters and electron density model follows.

### 3. MODEL FOR SOLAR ZENITH ANGLE

The model for  $f_o E$  requires the solar zenith angle. From the law of cosines of a spherical triangle, this quantity is given by:

$$\cos Z = \sin \delta \sin \theta + \cos \delta \cos \theta \cos (\phi - \phi_s), \quad (1)$$

where

$Z$  is the solar zenith angle,

$\delta$  is the solar declination (=latitude of the subsolar point),

$\phi_s$  is the east longitude of the subsolar point,

$\theta$  is the geographic latitude of the field point,

$\phi$  is the east longitude of the subsolar point.

The field point  $(\theta, \phi)$  is given, and the subsolar point  $(\delta, \phi_s)$  is required.

The subsolar point may be determined from the solution of the Kepler problem using mean elements from the American Ephemeris and Nautical Almanac. Such a solution, to second order in the eccentricity of the earth's orbit and neglecting lunar perturbations, produces an ephemeris accurate to within a nautical mile.

Alternatively, a simplified model for the solar ephemeris may be constructed, accurate to one degree of arc, as follows:

$$\delta = E \sin \Lambda, \quad \Lambda = 2\pi(d-80)/365.25, \quad (2)$$

$$\phi_s = \pi - UT,$$

where,  $E$  is the obliquity of the earth's equator ( $\approx 23.45$ ),  $\Lambda$  is the mean longitude of the sun measured in the ecliptic counterclockwise from the first point of Aries, UT is the universal time, and  $d$  the day of year.

Clearly, models between these two may be constructed; in particular, the annual variation of the equation of time may be modelled as a correction to the subsolar longitude. (The equation of time is the correction to be added to "sundial time" to reduce it to local mean time.) Such an approach is used in the WIMP program, with the following algorithm implemented in subroutine PTHP each time it is called. The solar declination ("zenith correction angle for day of year") is approximated by:

$$\delta' = E \sin (2\pi(d-82.5)/364) . \quad (3)$$

The equation of time in hours is modelled by:

$$X_j = aY^* [A_1/(B_1 + X_1)] - [A_2/(B_2 + X_2)] , \quad (4)$$

where

$$\begin{aligned} a &= 0.0235 \text{ hours;} \\ Y &= +1. , X_2 = d + 21. , \quad 0.0 < d < 162.5 ; \\ Y &= -1. , X_2 = 344.5 - d, \quad 162.5 \leq d < 344.5 ; \\ Y &= +1. , X_2 = d - 344.5, \quad 344.5 \leq d < 366.5 ; \\ X_1 &= (X_2/45.)^3; \\ A_1 &= 64. , A_2 = 240. , B_1 = 4. , B_2 = 15. \end{aligned}$$

The following angle is defined,  $X_j$  being converted to radians:

$$D = \phi' + X_j - \phi , \quad (5)$$

where

$$\phi' = \pi - UT, \quad UT \geq \pi ,$$

$$\phi' = \pi + UT, \quad UT < \pi .$$

The following approximation to the solar zenith angle is constructed:

$$Z_a^2 = \left[ (D \cos(0.6(\phi + \delta'))) \right]^2 + (\theta - \delta')^2 , \quad (6)$$

and the cosine of the solar zenith angle is approximated by:

$$\cos Z = \cos (0.932 Z_a) . \quad (7)$$

In the above description, angles are considered in radians, including UT; furthermore, longitudes are conventionally taken to be positive east. In the coding of PTHP, angles are conventionally in degrees, UT in hours, and longitudes are positive west.

#### 4. MODEL FOR THE E-LAYER PARAMETERS

The E-layer critical frequency  $f_E$ , layer height  $h_E$ , semithickness  $y_E$ , and bottom altitude  $h_b$  are required. If the simple parabolic E-layer model is selected,

$$\begin{aligned} h_b &= 100 \text{ km}, \\ h_E &= 115 \text{ km}, \\ y_E &= 15 \text{ km}. \end{aligned} \quad (8a)$$

If, on the other hand, the "parabolic E- with D-layer tail" electron density model is selected,

$$\begin{aligned} h_b &= 100 - 4 \cdot F_1 F_2, \\ h_E &= 115 \text{ km}, \\ y_E &= h_E - h_b. \end{aligned} \quad (8b)$$

where

$$\begin{aligned} F_1 &= 1 - (1 - R/3000)^2 & R < 6000 \text{ km}; \\ F_1 &= 0 & R \geq 6000 \text{ km}; \\ F_2 &= \cos(A) & A < \pi/2; \\ F_2 &= 0 & A \geq \pi/2; \\ R &= \text{DIST}(\theta, \phi, 76.0^\circ \text{ N}, 102.0^\circ \text{ W}); \\ A &= \phi + \frac{1}{2} |t - \pi| - \frac{1}{2} \pi; \end{aligned}$$

and  $(\theta, \phi)$  is the geographic north latitude and east longitude of the field point; DIST is the great circle distance (in km) between the two points specified in the argument list.

The critical frequency  $f_E$  is modelled from the sunspot number  $N_s$  and the cosine of the solar zenith angle  $\cos Z$  [as modelled by Eq. (7)]. Let

$$C_1 = \frac{1}{4} (1 + \cos Z)^2, \quad S_1 = (1 + 0.004 N_s)^{\frac{1}{2}},$$

$$f_n = 0.75 S_1 C_1, \quad f_x = 3.17 S_1 (\cos Z)^a, \quad (9a)$$

$$f_d = (f_x^2 + f_n^2)^{\frac{1}{2}}, \quad a = 1/3.775.$$

Then, at night ( $\cos Z$  negative)  $f_E$  is given by  $f_n$ ; during the day ( $\cos Z$  positive)  $f_E$  is given by  $f_d$ , unless  $f_d$  exceeds  $f_2$  ( $f_oF_2$  as modelled by the ITS-78 model) in which case  $f_n$  is taken. Furthermore,  $f_E$  is constrained not to exceed

$$f_{E \max} = (0.99 f_2 - 0.5)/1.26. \quad (9b)$$

## 5. MODEL FOR THE $F_1$ -LAYER CRITICAL FREQUENCY

The  $F_1$ -layer critical frequency  $f_1$  is given by

$$f_1 = 0.5 + 1.26 f_E, \quad (10)$$

(10)

and is constrained [Eq. (9b)] not to exceed  $0.99 f_2$ .

## 6. MODEL FOR $f_oF_2$ AND $M(3000)F_2$

These two parameters,  $f_2$  and  $M_3$ , are given by the ITS-78 parameter prediction model. This model is sufficiently well known that it will not be described in detail herein. Generally, the model consists in reducing a set of coefficients for each modelled parameter to a given phase of the solar cycle, season of the year, universal time, and geographic position. The solar cycle is represented by the sunspot number, and the parameters are fitted to a first or second order polynomial. The seasonal variation of the various parameters is represented by different sets of coefficients for each month, except for  $f_oF_2$ . The latter is represented as a Fourier sum (9 terms) in the day of the year. The diurnal variation is represented by a Fourier expansion (up to 13 terms) and the global variation is represented by a (modified) spherical harmonic expansion. Parameters modelled are  $f_oF_2$ ,  $M(3000)F_2$ ,  $h_pF_2$ ,  $f_oE$ , upper decile  $f_oE_s$ , median  $f_oE_s$ , and the lower decile  $f_oE_s$ . Only the first two parameters are used herein.

## 7. MODEL FOR THE F<sub>2</sub>-LAYER SEMITHICKNESS

The F<sub>2</sub>-layer semithickness  $y_2$  is given by

$$y_2 = F_y (56 + 0.489 N_s) . \quad (11)$$

The model allows for a correction scale factor  $F_y$ , which is initialized to unity; no provision is made for its redefinition.

## 8. MODEL FOR THE F<sub>2</sub>-LAYER HEIGHT

The model employed for the construction of the F<sub>2</sub>-layer height uses all of the parameters thus far described:  $f_E$ ,  $f_1$ ,  $f_2$ ,  $M_2$ ,  $y_2$ ,  $h_b$ ,  $h_m$ . The following frequencies are defined:

$$\begin{aligned} f'_q &= f_2 - \frac{1}{4} (f_2 - f_1), \\ f''_q &= f_2 - 0.01 f_2 y_2, \\ f_q &= \max (f'_q, f''_q), \\ f_3 &= f_2 M_3, \\ f_o &= 4 f_q - 3 f_2, \\ f_a &= f_o + 3.78 f_E + 1.5, \\ f_b &= 1.26 f_E + 0.5, \\ f_c &= f_o + 8.82 f_E + 3.5, \\ f_d &= f_o - 1.26 f_E - 0.5 = f_o = f_1, \\ f_e &= 8.00 f_E, \\ f_f &= f_o + 7.78 f_E + 1.5, \\ f_h &= f_o - 0.22 f_E + 1.5, \\ f_i &= f_2 + f_q, \\ f_j &= f_2 - f_q. \end{aligned} \quad (12)$$

The following parameters are defined (these are stored for later use in the construction of the M(3000)F<sub>2</sub> correction factor;

$$\begin{aligned} H_3 &= 70 + 3100 (f_q/f_3)^2, \\ F_q &= f_q/f_2, \end{aligned} \quad (13)$$

$$\begin{aligned}
P_3 &= (f_a/f_b) \log (f_c/f_d), \\
Z_1 &= y_E (f_a/f_e) \log (f_f/f_h), \\
Z_2 &= \frac{1}{2} y_2 (f_q/f_2) \log (f_i/f_j).
\end{aligned}$$

The  $F_2$ -layer height is given by:

$$h_2 = 8.0 (H_3 - Z_1 - Z_2 - h_b) / P_3 + y_2 + h_E. \quad (14)$$

#### 9. MODEL FOR THE $F_1$ -LAYER HEIGHT AND SEMITHICKNESS

The  $F_1$ -layer height  $h_1$  and semithickness  $y_1$  are given by:

$$\begin{aligned}
h_1 &= h_2 - y_2, \\
y_1 &= h_1 - h_E.
\end{aligned} \quad (15)$$

#### 10. MODEL FOR $F_2$ -LAYER CORRECTION FACTORS — VERTICAL IONOGRAM

The following information had been extracted from a vertical incidence ionogram as input to the program from which correction factors to the  $F_2$  layer parameters are to be derived:

- $t_r$  — universal time of ionogram,
- $L_r$  — geographic north latitude of sounding station,
- $W_r$  — geographic west longitude of sounding station,
- $F_1$  —  $f_o F_1$  from ionogram,
- $F_2$  —  $f_o F_2$  from ionogram,
- $F_q = F_1 + \frac{1}{4} (F_2 - F_1)$ ,
- $F'_q = F_2 - \frac{1}{4} (F_2 - F_1)$ ,
- $H_v$  —  $F_2$  virtual height at frequency  $F_q$ ,
- $H'_v$  —  $F_2$  virtual height at frequency  $F'_q$ ,
- $N_s$  — sunspot number,
- $D_y$  — day of year.

The ionospheric parameters at the given event are constructed from the parameter prediction model; let these parameters be represented by the following notation:

- $f_E, f_1, f_2$  — critical frequencies,  
 $h_E, h_1, h_2$  — layer heights,  
 $y_E, y_1, y_2$  — semithickness,  
 $h_b$  — bottom of ionosphere,  
 $M_3$  —  $M(3000)F_2$ ,  
 $f_q$  — "quarter point frequency", Eq. (14),  
 $Z_1, Z_2, P_3$  — Eq. (15) parameters.

Define the following frequencies:

$$\begin{aligned}
 f'_q &= f_1 + \frac{1}{4} (f_2 - f_1), \\
 f_a &= f_2 + 3.78 f_E + 1.5, \\
 f_c &= f_2 + 8.82 f_E + 3.5, \\
 f_d &= f_2 - f_1, \\
 f_f &= f_2 + 7.78 f_E + 1.5, \\
 f_h &= f_2 - 0.22 f_E + 1.5, \\
 f_i &= f_2 + f'_q, \\
 f_j &= f_2 - f'_q.
 \end{aligned}$$

Define the following quantities:

$$\begin{aligned}
 Z'_1 &= (y_E/8) * (f_a/f_E) * \log (f_f/f_h), \\
 Z'_2 &= (y_2/2) * (f'_q/f_2) * \log (f_1/f_j), \\
 P'_3 &= (f_a/f_1) * \log (f_c/f_d), \\
 H'_3 &= (P_3/P'_3) * (H_v - Z'_1 - Z'_2 - h_b) + Z_1 + Z_2 + h_b, \\
 M'_3 &= (f'_q/f_2) * (3100/H'_3 - 70) \overline{2}.
 \end{aligned}$$

Then the correction factors  $R_f$  and  $R_m$  purporting to correct predicted  $f_oF_2$  and  $M(3000)F_2$  parameters are given by:

$$\begin{aligned}
 R_f &= F_2/f_2, \\
 R_m &= M'_3/M_3.
 \end{aligned} \tag{16}$$



## 11. MODEL FOR F<sub>2</sub>-LAYER CORRECTION FACTORS – OBLIQUE IONOGRAM

Factors FR and MR are calculated in one run of the OBLFACT program, and are used as input for the next run of OBLFACT to be stored in elements 3 and 5 of /PERTC/. The reference point is also input directly into elements 1 and 2 of /PERTC/; the remaining elements are established by DATA statements. In the following description, the elements of /PERTC/ are referenced by the elements of (C<sub>i</sub>; i=1, 16). The field point north latitude and west longitude (N,W) are arguments of PERTC, the algorithm for the calculation of the oblique correction factors. The reference latitude and longitude, C<sub>1</sub> and C<sub>2</sub>, are alternatively referenced as N<sub>r</sub> and W<sub>r</sub>, respectively.

The algorithm commences by computing the distance and azimuth to the field point (N,W) from the reference point (N<sub>r</sub>,W<sub>r</sub>); let these two quantities be D and Z<sub>o</sub>, respectively.

Define the following quantities:

$$\begin{aligned} Z &= Z_o - C_{16}, \\ Z_1 &= (\pi/180)*(C_{13} - C_{12} - 90), \\ S &= \csc(Z_1), \\ Y &= 3600 C_9 C_{11} S, \\ W &= C_{10} S \\ Z_2 &= (\pi/180)*((D + Y)/360 W), \\ X &= \sin(Z_2). \end{aligned}$$

The following correction factors are then calculated:

$$R_a = (1 + C_i X) * (1 + C_j D/C_k) * (1 + C_m Z) \quad (17)$$

where the f<sub>o</sub>F<sub>2</sub> and M(3000)F<sub>2</sub> corrections are specified by the index set (a; i, j, k, m) being assigned values (f; 7, 3, 4, 14) and (m; 8, 5, 6, 15), respectively. These factors are then applied to the appropriate F<sub>2</sub>-level parameter.

## 12. ELEMENTS OF COMMON BLOCK/PERTC/

This common block is linked to the INPUT file via NAMELIST inputs in the main programs MAIN and FTDBLB; OBLFACT links elements of NAMELIST input (FRO and MRO) as arguments of subroutines SKIP and/or PEAK; the latter two routines

then define elements 3 and 5 of /PERTC/ equal to FRO and MRO, respectively. OBLFACT also links the first two elements NLREF and WLREF to the input NAMELIST. All elements are assigned default values in a BLOCK DATA program; presumably, these defaults may be assigned different values by replacing the BLOCK DATA program. The elements of /PERTC/ are used by SUBROUTINE PERTC which computes additional corrections to  $f_o F_2$  and  $M(3000)F_2$  based on information extracted from an oblique ionogram. The reference point (NLREF, WLREF) is the same reference point used in the construction of the updating correction factors to  $f_o F_2$  and  $M(3000)F_2$  effected in SUBROUTINE FACTO.

Table 1. The Elements of /PERTC/ with the Mnemonic Names Used in PERTC and the Default Values Assigned in the BLOCK DATA Program

Element	Mnemonic	Default	Element	Nnemonic	Default
1	NLREF		2	WLREF	
3	FR	0.0	4	FD	1000.0
5	MR	0.0	6	MD	1000.0
7	FZ	0.0	8	MZ	0.0
9	DUT	0.0792	10	DW	148.5
11	X	0.225	12	GAMMA	180.0
13	AZM	38.808	14	DFAC	0.0
15	DMAC	0.0	16	AZREF	0.0

### 13. ELECTRON DENSITY MODEL

A continuous electron density profile is constructed from the predicted ionospheric parameters. Slope discontinuities may occur in the model at the critical points of the profile. The model allows for either a parabolic model for the lower E-layer (below the critical altitude) or an E-layer with a D-layer tail; these two models will be described first.

In the parabolic E-layer model, the base altitude, layer height, and semi-thickness are modelled to be 100, 115, and 15 km, respectively. Below the E-layer height  $h_E$ , the electron density  $N_e$  is given by:

$$\begin{aligned}
 N_e &= 12400 f_E^2 (1 - Y^2), \quad h_b < h < h_E; \\
 N_e &= 0, \quad h < h_b,
 \end{aligned}
 \tag{18}$$

where

$Y = (h_E - h)/y_E$ ;  $h$  is the altitude;  $h_E$ ,  $y_E$ , and  $f_E$  are the E-layer height, semithickness, and critical frequency.

In the E-layer/D-layer tail model the semithickness may increase by up to 4 km,  $h_b$  will lower correspondingly, and  $h_E$  remains at 115 km. First, an electron density  $N_{eo}$  is calculated by Eq. (20) with  $Y$ , however, constructed as follows:

$$\begin{aligned} Y' &= 2 (h_E - h)/y_E, \\ x &= 1.5 \left[ 1.7 / (1.7 + Y') \right]^{\frac{1}{2}}, \\ z &= \left[ 1 + 0.1 (Y' - 1) \left| Y' - 1 \right| \right] / \left[ 1 - 0.1 / (Y' + 1)^2 \right], \\ Y'' &= 2 - \log (1 + 1.72 (Y')^x), \\ Y &= 1, Y'' \text{ negative}, \\ Y &= 1 - \frac{1}{2} (Y'')^2, Y'' \text{ not negative}. \end{aligned}$$

Then

$$N_{eo} = 12400 f_E^2 (1 - Y^2). \quad (19)$$

Calculate the correction for the D-layer tail  $N_d$  as follows:

$C = \cos (0.85 X)$ , where  $X$  is the solar zenith angle;

$$\begin{aligned} N_d &= 0, C \text{ negative}; \\ N_d &= (1 + 0.004 N_s) C^{\frac{1}{4}} / (1 + 81 W^4); \end{aligned} \quad (20)$$

where

$W = (65 - h)/y_E$ , and  $N_s$  is the sunspot number.

The electron density is finally given by:

$$N_e = N_{eo} + N_d. \quad (21)$$

Between  $h_E$  and  $H_2$ , the plasma frequency  $F_p$  is taken as the positive solution of a quadratic equation:

$$aF_p^2 + bF_p + c = 0 \quad (22)$$

and the electron density is taken as

$$N_e = 12400 (F_p)^2. \quad (23)$$

The coefficients a, b, and c are calculated as follows:

First, define three reference heights  $h_a$ ,  $h_b$ ,  $h_c$ :

$$\begin{aligned} h_a &= h_1 - y_1 (1 - (f_E/f_1)^2)^{\frac{1}{2}}, \\ h_b &= h_2 - y_2 (1 - (f_1/f_2)^2)^{\frac{1}{2}}, \\ h_c &= \frac{1}{2} (h_1 + h_b). \end{aligned}$$

For  $h$  between  $h_E$  and  $h_c$ , define coefficients  $B_1$ ,  $B_2$ ,  $B_3$ ,  $B_4$  as follows:

$$\begin{aligned} B_1 &= \frac{1}{2} (h_a - h_E + h_b - h_1) / (f_1 - f_E), \\ B_2 &= (h_1) - \frac{1}{2} (f_1 (h_a - h_E) + f_E (h_b - h_1) / (f_1 - f_E), \\ B_3 &= y_1 / f_1, \\ B_4 &= y_1. \end{aligned}$$

For  $h$  between  $h_c$  and  $h_2$ , the  $B_i$ 's are given by:

$$\begin{aligned} B_1 &= \frac{1}{2} (h_b - h_1) / (f_2 - f_1), \quad B_2 = h_2 - f_2 B_1; \\ B_3 &= y_2 / f_2, \quad B_4 = y_2. \end{aligned}$$

The coefficients a, b, c of the quadratic Eq. (22) are defined as:

$$\begin{aligned} a &= B_1^2 + B_3^2, \\ b &= 2 B_1 (B_2 - h), \\ c &= (B_2 - h)^2 - B_4^2. \end{aligned}$$

The topside model ( $h$  greater than  $h_2$ ) is a modified Chapman profile. Let  $Y = 2 (h - h_2) / y_2$ ; then,

$$\begin{aligned} N_e &= 12400 \left\{ (f_2)^2 \exp [1 - Y - \exp (-Y)] \right. \\ &\quad \left. + (0.5 + 0.1 f_2) h_2 (h - h_2) / h^2 \right\}. \end{aligned} \quad (24)$$

#### 1.4. MODEL FOR THE GRADIENT OF THE ELECTRON DENSITY

Any ray-tracing technique will require the gradient of the electron density at a field point  $(r, \theta, \phi)$ . Clearly, the complications of the model described above for the electron density mitigate against any attempt to derive analytic expressions for the gradient, even neglecting variations in the ionospheric parameters. Furthermore, should one desire to replace the electron density model with some other, either more or less complicated, a general numerical algorithm for the gradient is desired.

The gradient model employed in the WIMP program places the field point at the center of a cubical volume, and computes the electron density at each of the nine points so defined. The coordinates of these nine points are listed in the following table.

Table 2. Coordinates of Points Used for Gradient Calculation

Point	Radial Coordinate	Theta	Phi
1	$r$	$\theta$	$\phi$
2	$r + D_r$	$\theta + D_\theta$	$\phi + D_\phi$
3	$r + D_r$	$\theta - D_\theta$	$\phi + D_\phi$
4	$r + D_r$	$\theta + D_\theta$	$\phi - D_\phi$
5	$r + D_r$	$\theta - D_\theta$	$\phi - D_\phi$
6	$r - D_r$	$\theta + D_\theta$	$\phi + D_\phi$
7	$r - D_r$	$\theta - D_\theta$	$\phi + D_\phi$
8	$r - D_r$	$\theta + D_\theta$	$\phi - D_\phi$
9	$r - D_r$	$\theta - D_\theta$	$\phi - D_\phi$

$(r, \theta, \phi)$  are the coordinates of the field point,

$(D_r, D_\theta, D_\phi)$  are the grid spacings,

$$D_\theta = D_r / r,$$

$$D_\phi = D_r / r \sin \theta.$$

Given a function  $f(x)$  evaluated at three points,  $x_0$ ,  $x_+ = x_0 + dx$ , and  $x_- = x_0 - dx$ , then the best estimate of the derivative of  $f$  at  $x_0$  is given numerically by:

$$f'_0 = \frac{1}{2} (f_+ - f_-) / dx \quad (25)$$

where  $f_-$ ,  $f_0$ , and  $f_+$  represent  $f(x_-)$ ,  $f(x_0)$ , and  $f(x_+)$ . The best estimate of the second derivative is given by:

$$f''_0 = \frac{1}{2} (f_+ - 2f_0 + f_-) / dx^2. \quad (26)$$

Unfortunately, the defined set of points does not contain quite the correct subset to implement the numerical model for the derivative specified by Eq. (25). However, appropriate partial derivatives may be evaluated at the center of each side of the defined cube. Each coordinate then has four approximations to the appropriate partial derivative of the electron density; for instance, the  $r$  partial derivative will use pairs (2, 6), (3, 7), (4, 8), and (5, 9).

The algorithm adopted to represent the partial derivatives is the average of the four approximate values.

The value chosen for the grid space is  $1/3-1/2$  km.

## 15. THE WIMP 3-D RAY-TRACING TECHNIQUE

The ray-tracing model employed in the WIMP program depends upon the application of Bouger's rule and parabolic electron density models in multiple layers; the gradient of the electron density at the reflection height is employed to determine the tilt of the reflecting layer.

The program allows for refraction and/or reflecting in the E,  $F_1$ , and  $F_2$  layers. The  $F_1$  layer is inserted between the E and  $F_2$  such that the bottom of the  $F_1$  layer is at the E-layer height and the  $F_1$ -layer height is at the bottom of the  $F_2$  layer.

The ray tracing is accomplished in SUBROUTINE TRISL.

### 15.1 Bouger's Rule

Bouger's rule states that in a refracting medium with spherical symmetry electromagnetic radiation propagates in such a way that the quantity  $\mu r \cos \beta$  remains constant where  $\mu$  is the local index of refraction,  $r$  is the distance to the field point from the center of symmetry, and  $\beta$  is the local elevation angle.

### 15.2 Refraction Through a Layer

Refraction through a layer is depicted in Figure 1. The group path correction  $\Delta P'$  phase path correction  $\Delta P$ , and range correction  $\Delta$  are given by

$$\begin{aligned} \Delta P' &= \left( \frac{y}{\sin \beta_c} \right) \left\{ \frac{1}{2} u \log \left( \frac{u+1}{u-1} \right) - 1 \right\}, \\ \Delta P &= \left\{ 1 - \frac{1}{2} \sin^2 \beta_c (1 + 1/u^2) \right\} \Delta P' - \frac{1}{2} y \sin \beta_c / u^2, \\ \Delta &= \Delta P' \cos \beta_c / (R_0 + h_m), \end{aligned} \quad (27)$$

where  $u = f \sin \beta_c / f_c$  and  $f$  is the operating frequency,  $f_c$  the critical frequency,  $R_o$  the radius of the earth,  $h_m$  the layer height,  $y$  the layer semithickness, and  $\beta_c$  the local elevation angle of the unrefracted ray at the layer height.

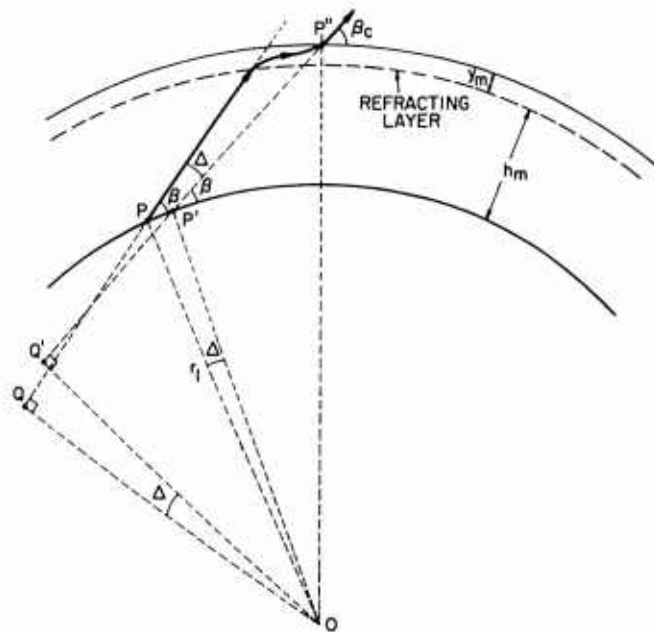


Figure 1. Refraction Through Layer

The group path length  $P'$  and phase path length  $P$  upon exiting the layer are given by

$$\begin{aligned} P' &= D_o + \Delta P', \\ P &= D_o + \Delta P, \end{aligned} \tag{28}$$

where  $D_o$  is the distance  $P'P''$  in Figure 1.

### 15.3 Reflection from a Layer

Reflection from a layer is depicted in Figure 2. The group path corrections  $\Delta P$  are given by

$$\Delta P' = \frac{y}{\sin \beta_r} \frac{1}{2} u \log \frac{u+1}{u-1},$$

$$\Delta P = \frac{1}{2} y \sin \beta_r + \left\{ 1 - \frac{1}{2} \sin^2 \beta_r (1 + 1/u^2) \right\} \Delta P',$$
(29)

where  $u = f \sin \beta_r / f_c$ , and  $\beta_r$  is the local elevation angle at the virtual height  $P''$ . These corrections apply for the upward trace to the reflection point; equal corrections obtain for the downward trace.

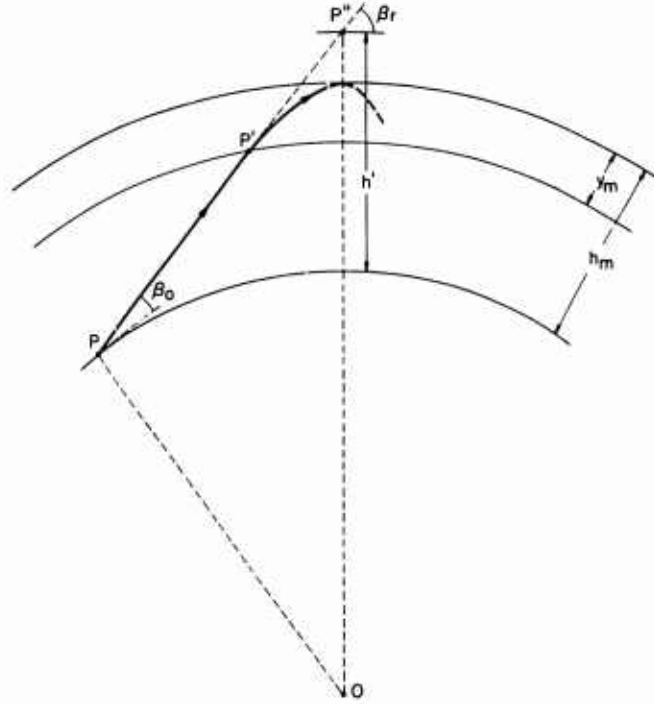


Figure 2. Reflection From Layer

#### 15.4 Tilted Reflection Layer

The gradient of the electron density at the ray reflection point is evaluated and employed to construct an effective tilted reflecting layer. Underlying refracting layers are considered concentric with the earth; however, gradients in these layers are taken into account in that the upward and downward legs of the ray trace through the underlying layers are spatially separated.

The introduction of a tilted reflecting layer, of course, generates considerable complication in the ray trace in that the ray direction, layer normal, and radius vector are no longer coplanar. The program accounts for these bookkeeping complications by setting up orthonormal triads as the ray attacks successive layers.



The y axis is taken parallel to the ray direction. The yz plane contains the center of curvature of the tilted reflecting layer (or the center of the earth in a refracting layer).

#### 15.5 Iteration Scheme

In each hop of the ray trace, the various calculations are iterated to refine the location of the profiles at which refraction through a layer and reflection from a layer occur. In the reflecting layer, the layer tilt is included within the iteration scheme.

At each stage of the ray-trace tests are made for pathological cases such as convergence failures in the allotted number of iterations, inconsistencies between stages, extremely tilted reflecting layers, ducting of the ray between layers, and so forth. Error diagnostic messages are printed prior to returning the main program should TRISL be required to abort the task.

### 16. FUNCTIONAL DESCRIPTION OF PROGRAM OBLFACT

#### 16.1 Initialization (Block 1)

This part of the program clears the INPUT file (NAMELIST INPUT). The elements of the NAMELIST are listed in Table 3 including the mnemonic name used, definition, and default value. A call to RIIP clears the INPUT file of the ITS parameter prediction coefficients. A call to FACTO calculates the  $F_2$  layer correction factors from  $f_oF_2$  and  $h'_{min}F_2$  scaled from the vertical ionogram and appearing in the NAMELIST input. Successive calls to PEAK and SKIP with the remote correction factors  $FR\phi$  and  $MR\phi$ , calculated from a previous run of OBLFACT, check that the ray tracing proceeds as expected (ground-to-ground mode). If not, the mission is aborted and the next task is initiated.

Table 3. Elements of NAMELIST/INPUT/

Mnemonic	Definition	Unit	Notes
SN	Sunspot Number		UNDEF
YRMD	Year & Month, concatenated		UNDEF
DOY	Day of Year	day	UNDEF
ZT	Universal Time, Vertical Ionogram (VI)	hours	UNDEF
RI	Geocentric Distance, VI	km	6370.
NL1	North Latitude, VI	degrees	
WL1	West Longitude, VI	degrees	

Table 3. Elements of NAMELIST/INPUT/ (Cont)

Mnemonic	Definition	Unit	Notes
ZIREF	Universal Time, Oblique Ionogram (OI)	hours	UNDEF
RS	Geocentric Distance to ray end point	km	5370.
NLREF	North Latitude, OI Sounder	degrees	
WLREF	West Longitude, OI Sounder	degrees	
AZ	Bore sight azimuth	degrees	
ELSTEP	Elevation step for SKIP search	degrees	1.0
FCF2R	$f_o F_2$ from VI	MHz	UNDEF
HMINR	$h'_{min} F_2$ from VI	km	UNDEF
FP	Peak Frequency	MHz	*
DELP	Peak Group Path Error	km	*
FS	Skip Frequency	MHz	*
DELS	Skip Group Path Error	km	*
DCIK	Tolerance in Group Path Deviations		10.0
MR $\phi$	Gradient Correction Factor, $M(3000)F_2$		$\neq$
FR $\phi$	Gradient Correction Factor, $f_o F_2$	MHz	$\neq$
MODE	MODE  = number of hops		?
IRSTRT	Termination Flag (STOP if $\phi$ )		1

Explanation of Terms Used in Table 3

- NOTES - A numerical value of this column is the default value set in OBLFACT.
- UNDEF - Implies that OBLFACT does not establish a default value.
- \*
- These values are determined from a comparison between the observed oblique ionogram (OOI) and the predicted oblique ionogram (POI) generated from a previous run of the BLOBZ driving program. Refer to "Step 5" of the Operating Instructions. Default values of  $\phi$  are assigned to F $\phi$  and DELP.
- $\neq$
- For the first run of OBLFACT, these parameters are set to  $\phi$ . Corrected values will be part of the output of OBLFACT to be used as inputs of a new run of OBLFACT at the user level of iteration. Refer to Steps 4 to 7 of the Operating Instructions.
- ?
- This parameter is an element of the argument list of the ray tracing program TRISL. Neither the operating instruction or the program flow chart illuminate the meaning of its sign. OBLFACT assigns a default value of -1.

### 16.2 Refinement of MR (Block II)

This part of the program iterates calls to PEAK in order to refine the  $M(3000)$  gradient correction factor MR. Since the peak frequency depends on antenna pattern and, thus upon elevation, it therefore depends primarily on the height of the layer. The Block II iteration maintains the  $f_o F_2$  gradient correction factor fixed. The value of MR is adjusted initially by 0.001 and subsequently by a Newton iterative technique until the predicted peak group path agrees with that from the oblique ionogram to within the specified tolerance (DCIK, nominally 10 km), at which point transfer is made to Block III.

Block II is ultimately reentered from Block IV after refinement of the  $f_o F_2$  gradient correction factor. A call to PEAK establishes whether further refinement is required. If the resultant group path is within tolerance, the task is terminated and the results printed.

Should the required information to effect this refinement be not available, the default values of 0 assigned to FP and DELP automatically cause this part of the program to be bypassed. Thus, only the  $f_o F_2$  gradient correction is determined; the  $M(3000)F_2$  gradient remains by default the same as that of the parameter model (ITS-78), which, presumably, is the best available in the absence of evidence to the contrary.

### 16.3 Refinement of FR (Block III and IV)

This part of the program iterates calls to SKIP in order to refine the  $f_o F_2$  gradient correction factor FR. In SKIP, rays are traced at frequency FS from  $0^\circ$  to  $20^\circ$  in steps given by ELSTEP (nominally  $1^\circ$  and must not be less than  $1/2^\circ$ ). The array of group paths is searched to locate the minimum. This is compared with the minimum group path extracted from the leading edge of the oblique ionogram at frequency FS. If the difference is within tolerance, the MR iteration is reentered. If not, FR is corrected for the next iteration.

Since OBLFACT is in a late user stage of simulation and a previous stage BLOB 2 produces the general ray-trace results, the user should have limiting information on the elevations between which the minimum group path should be located. The built-in  $0^\circ$  to  $20^\circ$  may not be sufficient to properly locate the minimum group path. The using facility might consider modifying the program to allow the user to specify the elevation domain to be searched. This may be accomplished as follows:

- (a) Link the initial elevation, ELBEG and number of elevations to be traced, NELM to NAMELIST/INPUT/ in OBLFACT.
- (b) Add ELBEG and NELM to COMMON/FIDDLE/ in OBLFACT, SKIP, and PEAK.

(c) Modify the elevation DO loop in SKIP as follows:

PRESENT VERSION	RECOMMENDED VERSION
NELM=20, D0/ELSTEP + 1, D0	(delete)
.	
.	EL=ELBEG
DO 10 IEL=1, NELM	DO 10 IEL=1, NELM
EL=(IEL-1)* ELSTEP	.
.	.
.	.
.	.
.	.
.	.
10 CONTINUE	10 EL=EL + ELSTEP

## 17. SUBROUTINE PEAK (FRR, MRR, GPP, IGOBAK)

### 17.1 Argument List

FRR -  $f_o F_2$  correction quantity (INPUT)  
MRR -  $M(3000)F_2$  correction quantity (INPUT)  
GPP - Predicted peak group path (OUTPUT)  
IGOBAK - Error condition returned (OUTPUT)

### 17.2 Common Blocks

/PERT C/ linked to PERT F, the routine that calculates  $F_2$ -layer correction factors from parameters scaled from the oblique ionogram.

/REMVEN/ linked from TRISL. Contains reflection layer information.

/FIDDLE/ linked from OBLFACT. Contains the "peak frequency" FP scaled from the oblique ionogram, transmitter location, and take-off azimuth.

### 17.3 Function

Computes the "predicted peak group path" corresponding to oblique ionogram correction factors FRR and MRR, and "peak frequency" FP.

### 17.4 Algorithm

The input parameters FRR and MRR are stored in elements 3 and 5 of /PERT C/ for use by PERT F for calculating correction factors to  $f_o F_2$  and  $M(3000)F_2$ .

An elevation is selected from the following critical table according to the peak frequency, element 1 of /FIDDLE/:

Table 4. Elevation Determination

FP less than	Elevation	FP less than	Elevation
5.74	Undefined	16.74	5.2
6.74	11.9	17.74	4.8
7.74	10.3	18.74	4.5
8.74	8.9	19.74	4.2
9.74	7.7	20.74	4.0
10.74	6.7	21.74	3.8
11.74	5.9	23.74	3.7
12.74	5.2	25.74	3.6
13.74	4.6	28.74	3.5
14.74	4.1	30.74	3.4
15.74	3.9	$\geq 30.74$	Undefined

The calling program is required to insure that  $5.74 < FP < 30.74$ .

The ray-tracing program TRISL is called to compute the predicted peak group path GPP.

Elements of /REMWEN/ are checked to insure reflection consistency occurs in the F2 layer. Furthermore, the geocentric distance of the ray endpoint is checked that it is less than 6378.85 km. If these tests are passed, the error condition flag IGOBAK is set to zero; otherwise, an error condition is noted by setting IGOBAK to unity.

#### 18. SUBROUTINE SKIP (FRR, MRR, GPS, IOPT, IGOBAK)

##### 18.1 Argument List

- FRR -  $f_o F_2$  correction quantity (INPUT)
- MRR -  $M(3000)F_2$  correction quantity (INPUT)
- GPS - Predicted minimum group path (OUTPUT)
- IOPT - Correction control parameter (INPUT)
- IGOBAK - Error condition returned (OUTPUT)

##### 18.2 Common Blocks

- /PERT C/ linked to PERT F
- /REMWEN/ linked from TRISL
- /FIDDLE/ linked from calling program (OBLFACT)

### 18.3 Function

Computes the predicted minimum group path corresponding to the oblique ionogram correction terms FRR and MRR, and "skip frequency" FS (element 2 of /FIDDLE/).

### 18.4 Algorithm

SKIP transfers FRR and MRR of the argument list to elements 3 and 5 of /PERT C/ respectively, to be used in /PERT F/ to calculate  $F_2$  correction factors.

A sequence of elevations between  $0^\circ$  and  $20^\circ$  is selected for ray tracing via calls to TRISL. The elevation step is contained in element 8 of /FIDDLE/ and a sufficient number of elevations are selected to include the entire domain ( $0^\circ$ ,  $20^\circ$ +). Provision is made for up to 41 ray traces; thus, the user must insure that the elevation step size is no greater than  $0.5^\circ$ . The elevation scan is terminated at the first occurrence of a penetration through the ionosphere if such occurs before the normal loop termination.

The rays traced in this elevation scan are partitioned into three sets:

- (a) Rays not reflecting from the  $F_2$  layer. These are excluded from further consideration in (b) and (c).
- (b) Rays with end point at geocentric distance no greater than 6378.85 km.
- (c) Rays with end point at geocentric distance greater than 6378.85 km.

If set (b) is empty, the error flag IGOBAK is set to unity and control is returned to the calling program. Otherwise, the element of (b) with the smallest group path is determined. This least group path is established as the predicted minimum group path GPS unless the following conditions obtain:

- (a) SKIP had been called with IOPT not zero, and
- (b) The ray with next higher elevation belongs to set (c) and has a smaller group path length.

In the latter case, the minimum group path returned as GPS is given by:

$$GPS = G_b + \left\{ (G_c - G_b) / (R_c - R_b) \right\} (6378.85 - R_b),$$

where the G's and R's refer to group paths and end point geocentric distance, and the subscripts b and c refer to the above selected elements of set (b) and (c).

Should calls be issued to SKIP more than 100 times in any run of OBLFACT, the error flag is set to two and the task immediately aborted.

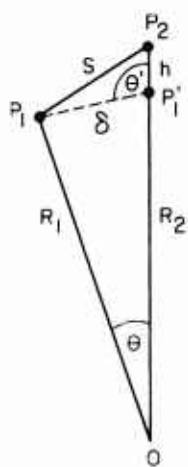
## 19. REMARKS ON THE USE OF DOUBLE PRECISION ARITHMETIC

The version of the program that the present author has studied has been modified from CDC 6600 machines for use on UNIVAC machines. The essence of this modification is to assign the double precision attribute to every real variable. In the opinion of the present author, wholesale use of double precision arithmetic is not justified, reduction notwithstanding.

In the first place, double precision arithmetic is expensive. Analysis of double precision arithmetic reveals that (1) twice the core storage is required for the variables involved in the calculation, (2) the coding requires, in general, three times the number of instructions, and (3) the execution time increases by approximately a factor of four.

In the second place, increasing the precision of a calculation does not increase the accuracy of the computed result. For example, the geomagnetic field employed in conjunction with the ITS parameter prediction model is a sixth order spherical harmonic expansion. The expansion coefficients are given to one part per million or less. An eight significant digit machine in single precision can calculate the geomagnetic field at a point to the accuracy of the model. The ionospheric parameter model is essentially a one percent model; double precision arithmetic will not improve this situation.

On the other hand, there are situations where single precision arithmetic may produce inaccurate results; for example, in the solution of plane triangles in certain situations.



Consider the situation depicted here. The distances  $R_1$  and  $R_2$  and the angle  $\theta$  are known and the distance  $S$  between  $P_1$  and  $P_2$  is required. The law of cosines applies and

$$S^2 = R_1^2 + R_2^2 - 2R_1 R_2 \cos \theta . \quad (30)$$

Typically, the distances  $R_1$  and  $R_2$  are of the order of 6000 km, the arc  $P_1P_1'$  might be 60 km ( $\theta = 0.01$  rad), and the altitude difference  $P_1'P_2'$  might also be of the order of 60 km. Thus, take  $R_2$  and  $\cos \theta$  to be given exactly by

$$R_2 = R_1(1 + 0.01),$$

$$\cos \theta = 1 - \frac{1}{2} \times 10^{-4} .$$

With single precision of 8 significant digits,

$$S^2 = R_1^2 - 1 + (1 + 2 \times 10^{-2} + 10^{-4} \pm 10^{-9}) - (2 + 2 \times 10^{-2} - 10^{-4} - 10^{-6} \pm 10^{-8})$$

$$S^2 = R_1^2 - 2 \times 10^{-4} + 10^{-6} \pm 10^{-8} .$$

In this case, the truncation error has resulted in reduction of precision to one part in  $10^4$ .

This loss of precision may or may not be tolerable; in either case it is not necessary, for the law of cosines may be reformulated to solve the triangle  $P_1 P_2 P'_1$  for  $S$ , retaining full single precision results. The length of the cord of the angle  $\theta$  is given by

$$\delta = 2R_1 \sin \frac{1}{2} \theta .$$

Furthermore,

$$\cos \theta' = - \sin \frac{1}{2} \theta = -\delta / 2R_1 ,$$

$$R_2 = R_1 + h .$$

Then,

$$S^2 = h^2 + \delta^2 + h\delta^2/R_1 . \quad (31)$$

This form of the law of cosines will retain single precision results, and should be used wherever possible. To implement this recommendation in SUBROUTINE TRISL, however, would require considerable effort and analysis; a totally new program may be required.

## 20. MODEL COMPARISON

For purposes of comparison, the WIMP program modelling subroutines were used to generate ionospheric models for various combinations of parameters (Sun-spot Number, Season, Universal Time) for a midlatitude location. These were compared with similar models derived from a program in use at RADC.<sup>4</sup> These comparisons are shown in Figures 3 through 13.

4. Rush, C. M., Miller, D., and Gibbs, J. (1974) The relative daily variability of  $F_oF_2$  and  $h_mF_2$  and their implications for HF radio propagation, Radio Science, 9:749-756.



Both models use the same formulation for  $f_oF_2$  - the maximum plasma frequency of the F-layer (the ITS-78 model). Figures 3 through 5 show the Universal Time variation of the height of maximum electron density ( $h_mF_2$ ) for three seasons and two sunspot numbers [W(XX) and R(XX) refer to the WIMP and RADC models for SSN = XX]. Similarly, Figures 6 through 8 show the comparison of parabolic semithickness ( $y_mF_2$ ); WIMP uses a semithickness value which is time independent. The WIMP model contains a discontinuity at the lower side of the F layer, which results in the most significant departures from the RADC model in the vertical profile. In order to illustrate these departures, the difference between the plasma frequency was calculated by the two models at the altitude of the  $F_1$ -layer maximum used in WIMP. These results are shown for four seasons in Figures 9 through 12, where the times of sunrise and sunset are also indicated. Figure 13 shows a comparison of the two models for given time ( $\chi$  is the solar zenith angle). The relevant ionospheric model parameters are indicated in the figure.

The results of ray tracing obliquely through the 3-D ionosphere of which Figure 13 represents a single vertical profile are shown in Figure 14. The ray-trace program used was the standard RADC program, known as ARCON II, ITS. As expected, the greatest discrepancies between the oblique group path for the WIMP and RADC models are to be found corresponding to the profile discontinuity at the  $F_1$  layer (compare Figures 9 through 12). In order to examine the differences in computed leading edge of a backscatter ionogram, due to the different models, a one-dimensional ionospheric model was generated, having the vertical profile given by the RADC and WIMP models in Figure 13, (that is, having no horizontal gradients). Leading edges were then computed for simulated backscatter ionograms, using the ARCON II ray-trace program, and the results shown in Figure 15.

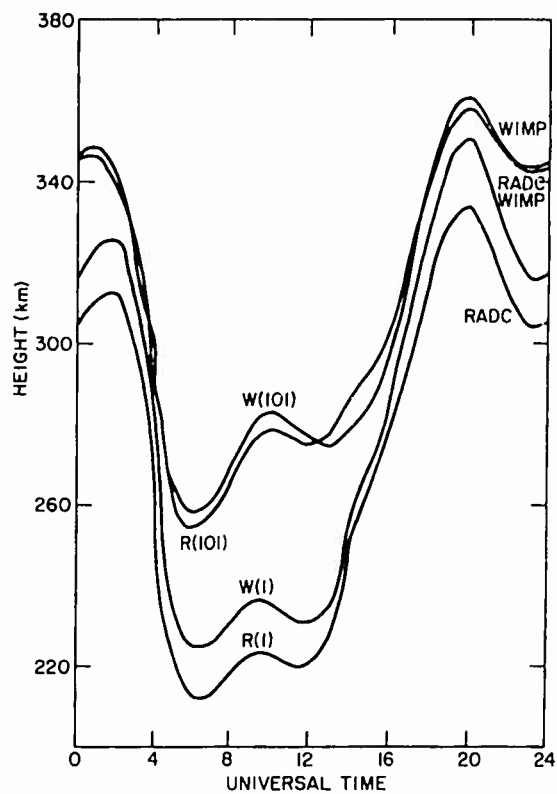


Figure 3. RADC and WIMP Model  $h_m F_2$ , Winter Solstice

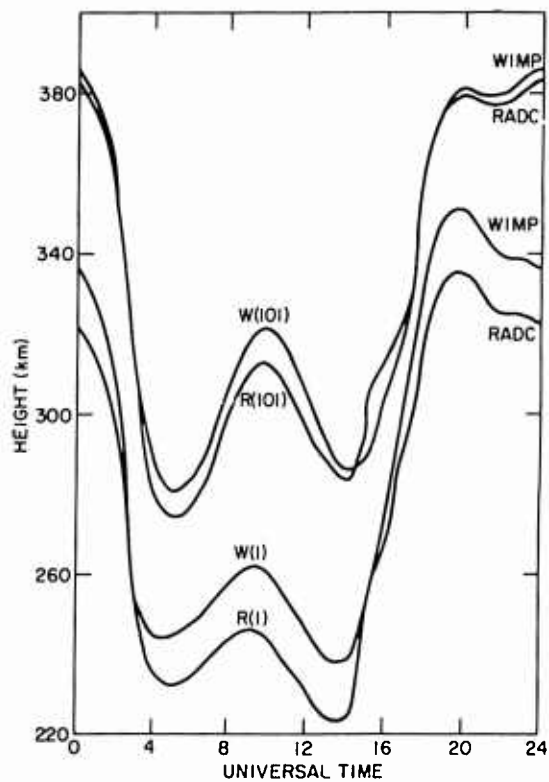


Figure 4. RADC and WIMP Model  $h_m F_2$ , Vernal Equinox

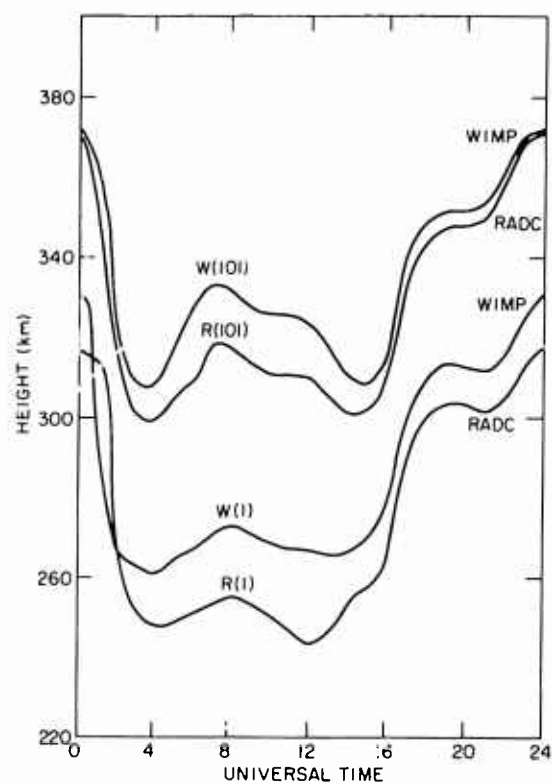


Figure 5. RADC and WIMP Model  $h_m F_2$ , Summer Solstice

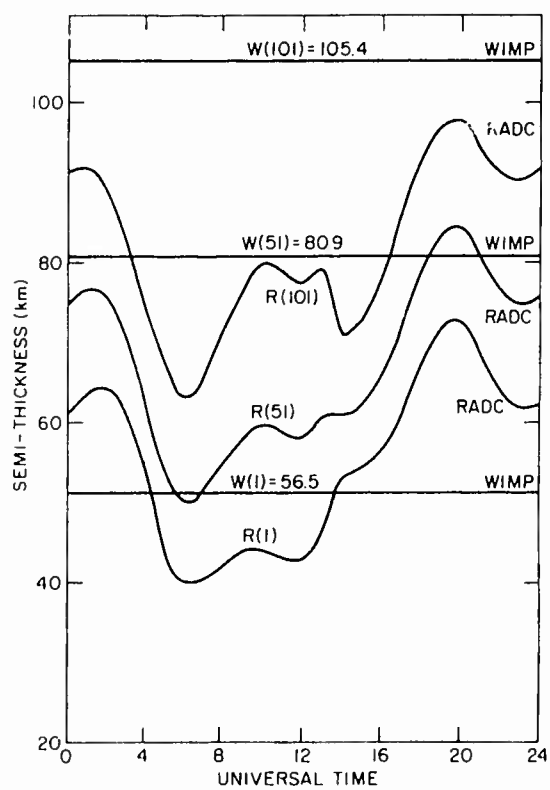


Figure 6. RADC and WIMP Model  $y_m F_2$ , Winter Solstice

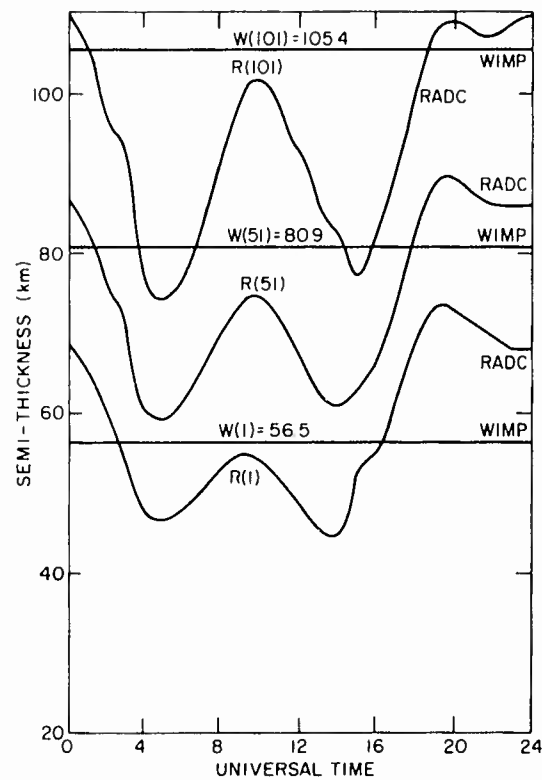


Figure 7. RADC and WIMP Model  $y_m F_2$ , Vernal Equation

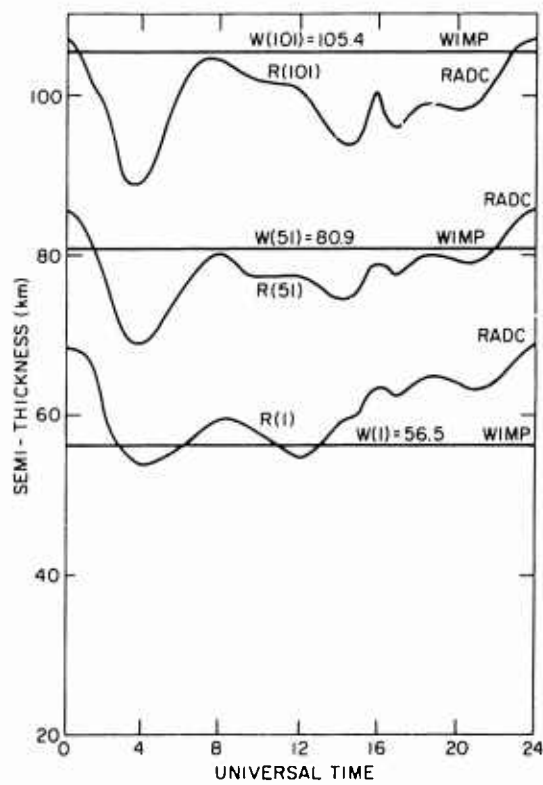


Figure 8. RADC and WIMP Model  $y_m F_2$ , Summer Solstice

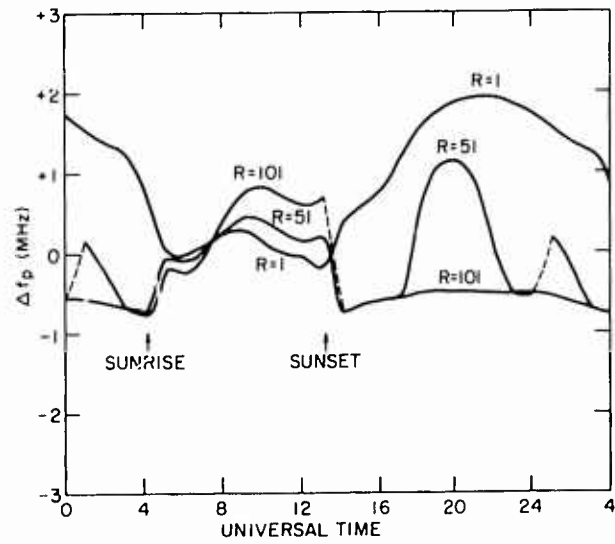


Figure 9. RADC Plasma Frequency at WIMP  $h_m F_1$  Minus WIMP  $f_o F_1$ , Winter Solstice

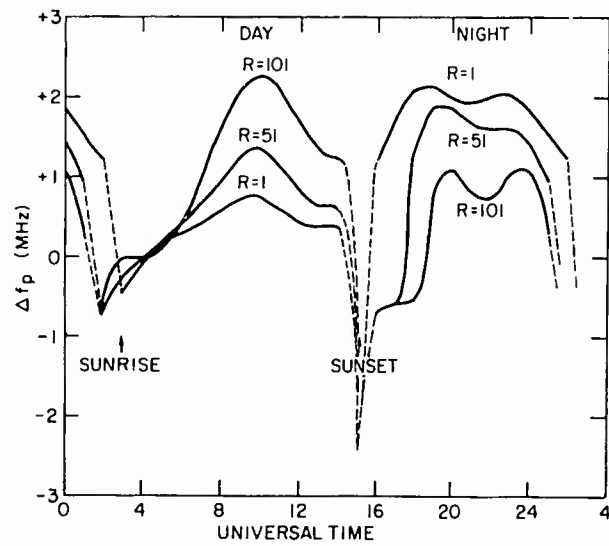


Figure 10. RADC Plasma Frequency at WIMP  $h_m F_1$  Minus WIMP  $f_o F_1$ , Vernal Equinox

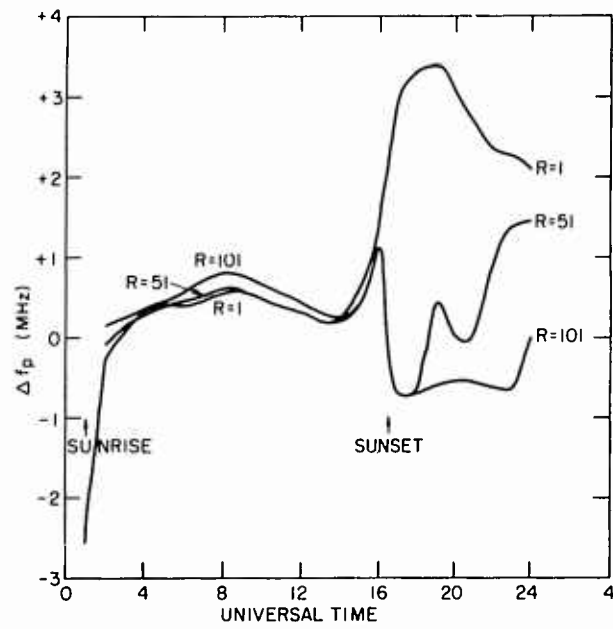


Figure 11. RADC Plasma Frequency at WIMP  $h_m F_1$  Minus WIMP  $f_o F_1$ , Summer Solstice

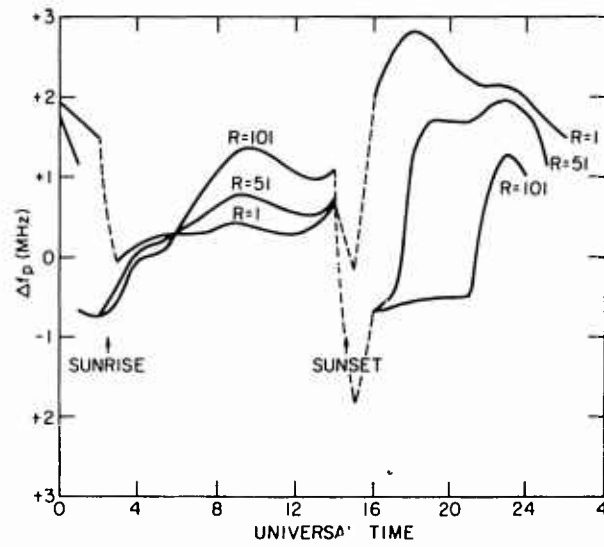


Figure 12. RADC Plasma Frequency at WIMP  $h_m F_1$  Minus WIMP  $f_o F_1$  Autumnal Equinox

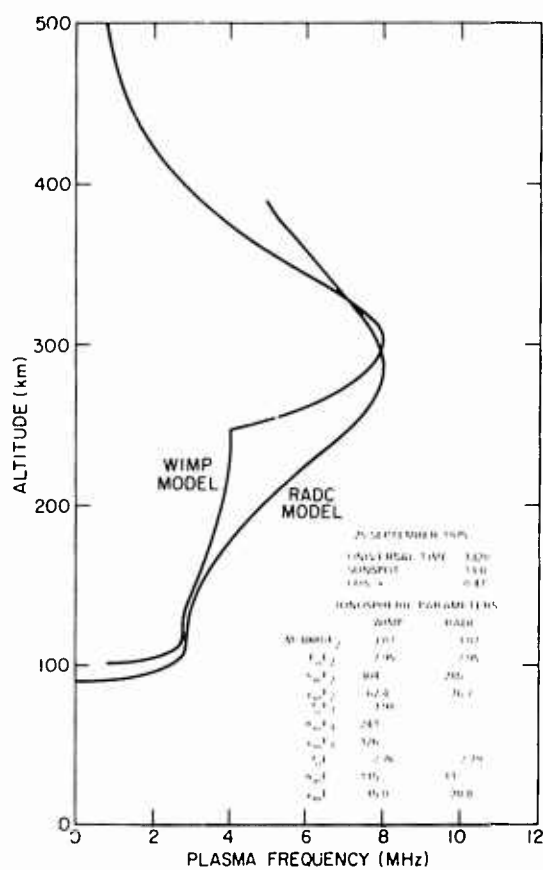


Figure 13. RADC and WIMP Plasma Frequency Profiles

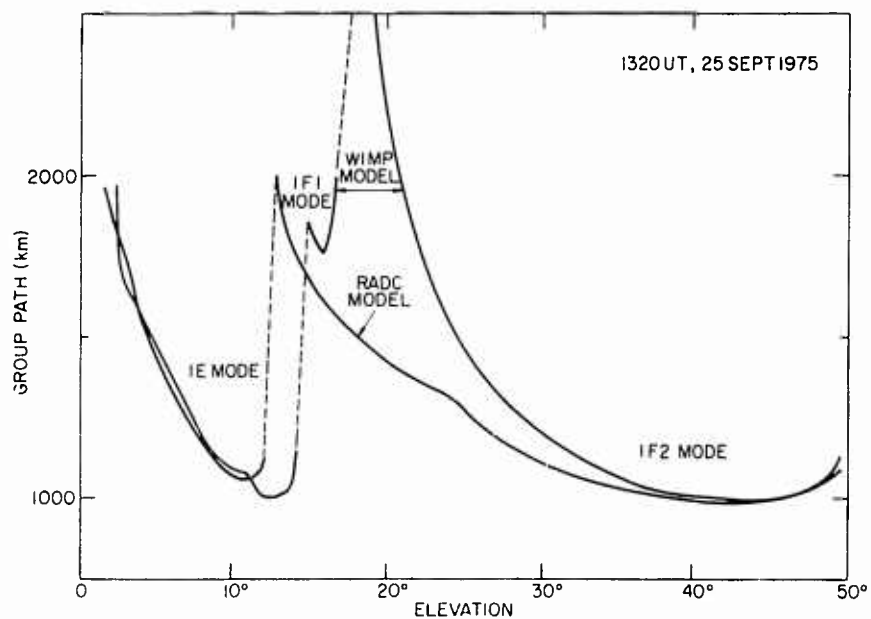


Figure 14. ALCON II 10-MHz Ray Traces, RADC and WIMP Profiles

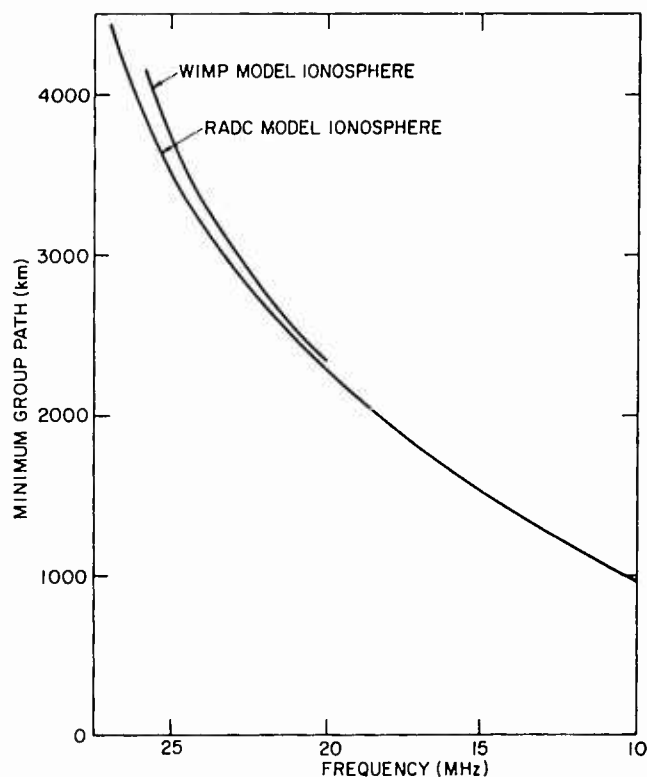


Figure 15. ARCON II  
Predicted Leading Edges,  
RADC and WIMP Profiles

## 21. COORDINATE CONVERSION

The conversion from apparent radar range (that is, group path ( $P$ ) to true range ( $R$ ) can be accomplished if the ionospheric structure is known, by using the procedures described earlier. The RADC model for 1320 UT on 25 September 1975 was used, together with the ARCON II ray-trace program, to compute ( $P$ - $R$ ) as a function of  $P$  for frequencies in the range 18 to 26 MHz, as shown in Figure 16. The locus of the backscatter leading edge is indicated by the curve labelled  $P_{\min}$ , corresponding to the minimum group path at each frequency.

Figure 17 shows the comparison of the actual leading edge of a backscatter ionogram measured at 1320 UT (Curve 2) with the simulated leading edge (Curve 6). Curve 1 shows a leading edge measured at 1340 UT, indicating that the ionosphere is moderately unstable, since Curves 1 and 2 are noticeably different. Curve 3 indicates a secondary leading edge appearing in the ionograms, perhaps a result of azimuthal gradients in the ionosphere. The ionospheric model was then updated by modifying it on the basis of the measured vertical ionogram and allowing for a linear gradient, such that

$$N_e = BN_{eo} (1 + A R_+),$$



where  $N_e$  is the modelled electron density at any location.

$N_{eo}$  is the modelled electron density (from the RADC program)

$$B = \frac{(f_o F_2)_{\text{measured}}}{(f_o F_2)_{\text{model}}},$$

$A = \text{constant},$

$R_+ = \text{boresight range (in radians)}.$

It should be noted that the range is here measured in terms of the angle subtended at the earth's center by the arc on the earth's surface which is the ground range. Curve 5 in Figure 17 shows the computed leading edge for  $A = 2.0$  and Curve 4 shows the best fit ( $A = 1.61$ ) with the measured data. By repeating the procedure illustrated in Figure 16, the best estimated conversion from radar range to true range can be determined for any operating frequency. Although azimuthal radar information is not available, it is possible to ray trace at various azimuths to establish a locus on the ground of possible ranges for a target having any given radar range.

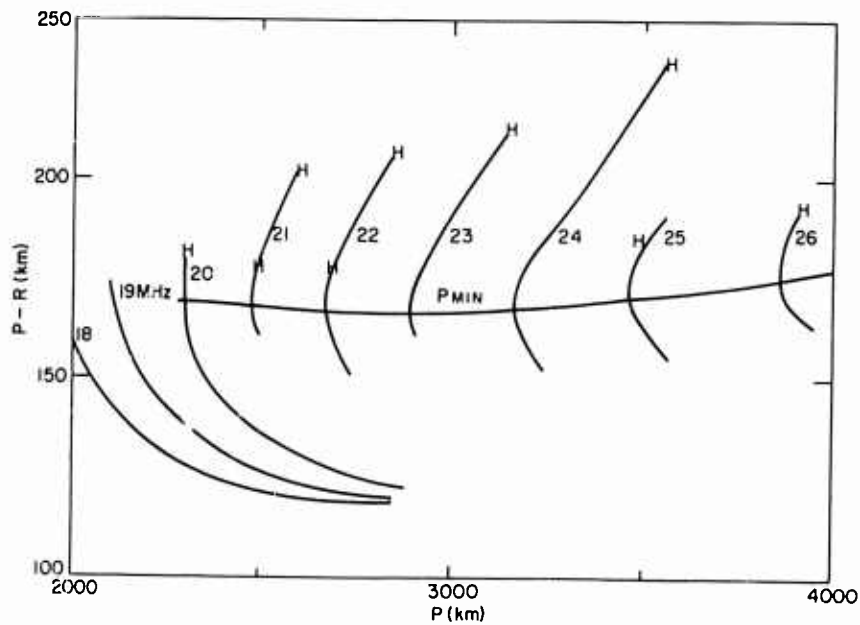


Figure 16. Illustrating Range Conversion

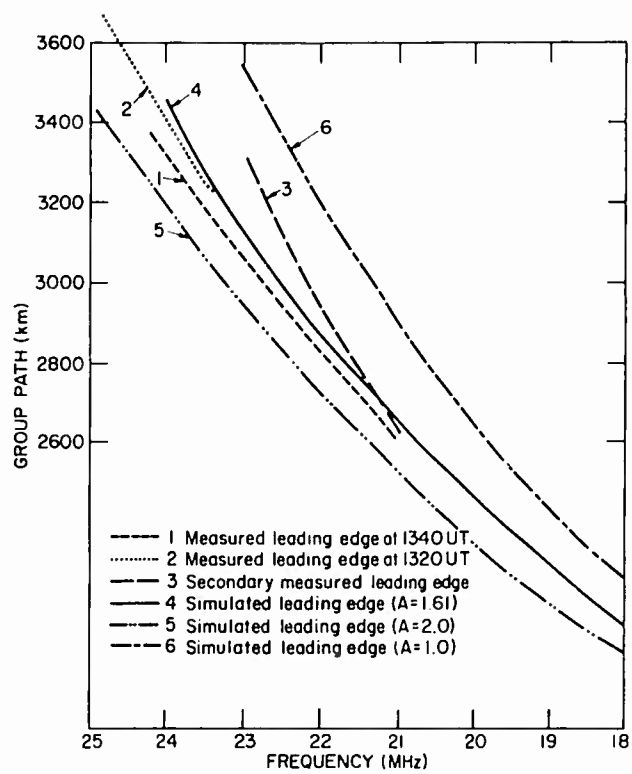


Figure 17. Backscatter Leading Edge Comparison

## Appendix A

### Program Listings for the WIMP Model Ionosphere

Program listings are included for the WIMP model ionosphere; each sub-routine is briefly described as follows:

1. RIIP - Calling control program for layer parameters and electron density.
2. CRPL2 - Generates  $f_oF_2$  and  $M(3000)F_2$ .
3. MMDIP - Geomagnetic Field Model.
4. PERT F -  $f_oF_2$  and  $M(3000)F_2$  gradient factors.
5. DFP3 - Great Circle Range/Azimuth Calculations.
6. DFP - Great Circle Range Calculation.
7. PTHP - E,  $F_1$ ,  $Y_m F_2$ , and  $h_m F_2$  calculations.
8. NFROMR - Electron Density Profile.

```

SUBROUTINE RIIP(RFEC,BNLATA,BWLONGA,PLASD)
C
C PROGRAMMED FOR D.ODOM BY COMPUTATIONS,INC. -OCTOBER,1967
C
C
C IMPLICIT DOUBLE PRECISION (A-H,O-Z)
C DOUBLE PRECISION M3000,NLATA
C DOUBLE PRECISION MFAC
C LOGICAL SMOOTH,TILT,NIP,FAST
C COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAЕ,HME,HAF1,HMF1,HAF2,HMF2,
1SN,ZT,YR,D,HAЕSET,MFAC,F2FAC,F1FAC,EFAC,H2FAC,SNSQRT,QRAD,CQ,IDL,I
2A,SMOOTH
C COMMON/RPERT/RRFEC,ITIP/NIPRIP/NIP/TILTC/TILT,FAST
C COMMON/RIIFWA/IX(4)
C REAL IX

DATA NLATA,WLONGA
DATA SN,ZT,YR,D/13.00,13.00,7509.00,269.00/
DATA M3000,FCF2,FCF1,FCE/3.0500,8.00,4.0800,2.7900/
DATA HBE,HME,HMF1,HMF2/90.00,110.00,180.00,288.00/
DATA HAE,HAF1,HAF2/20.00,70.00,108.00/
DATA MFAC,F2FAC,F1FAC,EFAC,H2FAC/5*1.00/
DATA HAЕSET/15.00/

NLATA=BNLATA*57.29577951308232D0
WLONGA=BWLONGA *57.29577951308232D0
RRFEC=RFEC
NLATA=DMOD(NLATA,90.00)
WLONGA=DMOD(WLONGA,360.00)+180.00-DSIGN(180.00,WLONGA)
1004 CALL CRPL2(NLATA,WLONGA)
M3000=M3000*MFAC
FCF2 = FCF2*F2FAC
C PREDICTED BOTTOM OF E LAYER
1005 BA=100.00
AA=BA+HAЕSET
IF(IDL*IA.EQ.0) GO TO 1006
CALL DFP(NLATA,WLONGA,76.00,102.00,DIST)
BA=100.00-4.00*DMAX1((1.00-DABS(DIST-3.03)/3.03)**2,0.000)*DMAX1(
1 DCOS((DABS(15.00*DABS(ZT-12.00)-WLONGA)-90.00)/(2.00*
2 57.29577951308232D0)),0.000)
C PREDICTED TRUE HEIGHT PROFILE
1006 CALL PTHP(NLATA,WLONGA,AA,BA)
C GET ELECTRON DENSITY AT REF. POINT
C GET N FROM R
IF(RFEC.LE.6370.00) RETURN
CALL NFROMR(RFEC,PLASD)
RETURN
END

```

OUTLINE CRPL2

74/74 OPT=1

FTN 4.5+414

04/27/

```

SUBROUTINE CRPL2(NLAT,WLONG)
C ...TO FIND CRITICAL FREQUENCY AS A FUNCTION OF THETA AND PHI
C FROM NEW NBS IONOSPHERIC PREDICTIONS FOR A PARTICULAR TIME...
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DOUBLE PRECISION NLAT,M3000,MFAC
DIMENSION SINTO(11),COSTO(11),G(76),GAMMA(2),DKTO(76,2)
DIMENSION CT(8),ST(8)
COMMON/RIIPAR/M3000,FCF20,DUM(9),SN,ZT,YR,DAY,HAESSET,MFAC,FFAC,
1DUM1(6),ID(3)
*/LABCRP/NHARM(2),KI(2),KII(2),KIII(2),KIV(2),KV(2),KVI(2),KVII(2),
*KVIII(2),KIX(2),D(13,76,2)
DATA RAD/.0174532925199433D0/
G(1)=1.0D0
CALL MMDIP(NLAT,WLONG,SSMX)
THERAD=(360.D0-WLONG)*RAD
COSLAM=DCOS(NLAT*RAD)
CT(1)=COSLAM*DCOS(THERAD)
ST(1)=COSLAM*DSIN(THERAD)
DO 63047 IJK=2,8
CT(IJK)=CT(1)*CT(IJK-1)-ST(1)*ST(IJK-1)
63047 ST(IJK)=CT(1)*ST(IJK-1)+ST(1)*CT(IJK-1)
IF(DABS(ZT-ZTP).LT.1.D-3.AND.DABS(YR-YRP).LT.1.D-1)GO TO 20
ZTP=ZT
YRP=YR
T0=15.000*ZT-180.000
TORAD=T0*RAD
ARG=0.0D0
NHARML=MAX0(NHARM(1),NHARM(2))
DO 1 J=1,NHARML
ARG=TORAD+ARG
SINTO(J)=DSIN(ARG)
1 COSTO(J)=DCOS(ARG)
DO 2 L=1,2
NHARML=NHARM(L)
K9=KIX(L)+1
DO 2 K=1,K9
DKTO(K,L)=D(1,K,L)
DO 3 J=1,NHARML
DKTO(K,L)=DKTO(K,L)+D(2*J+1,K,L)*COSTO(J)+D(2*J,K,L)*SINTO(J)
3 CONTINUE
2 DO 100 L=1,2
20 NHARML=NHARM(L)
K1=KI(L)+1
K2=KII(L)+1
K3=KIII(L)+1
K4=KIV(L)+1
K5=KV(L)+1
K6=KVI(L)+1
K7=KVII(L)+1
K8=KVIII(L)+1
K9=KIX(L)+1
K1P1=K1+1
K1P2=K1+2
K1P3=K1+3
K2P1=K2+1
K2P2=K2+2
K2P3=K2+3

```

	K3P1=K3+1	CRP
	K3P2=K3+2	CRP
	K3P3=K3+3	CRP
	K4P1=K4+1	CRP
	K4P2=K4+2	CRP
	K4P3=K4+3	CRP
	K5P1=K5+1	CRP
	K6P1=K6+1	CRP
	K7P1=K7+1	CRP
	K8P1=K8+1	CRP
	DO 4 K=2,K1	CRP
4	G(K)=G(K-1)*SSMX	CRP
	IF(K1.EQ.K2) GO TO 9	CRP
	G(K1P1)=CT(1)	CRP
	G(K1P2)=ST(1)	CRP
	DO 5 K=K1P3,K2,2	CRP
	G(K)=G(K-2)*SSMX	CRP
5	G(K+1)=G(K-1)*SSMX	CRP
	IF(K2.EQ.K3) GO TO 9	CRP
	G(K2P1)=CT(2)	CRP
	G(K2P2)=ST(2)	CRP
	DO 6 K=K2P3,K3,2	CRP
	G(K)=G(K-2)*SSMX	CRP
6	G(K+1)=G(K-1)*SSMX	CRP
	IF(K3.EQ.K4) GO TO 9	CRP
	G(K3P1)=CT(3)	CRP
	G(K3P2)=ST(3)	CRP
	DO 7 K=K3P3,K4,2	CRP
	G(K)=G(K-2)*SSMX	CRP
7	G(K+1)=G(K-1)*SSMX	CRP
	IF(K4.EQ.K5) GO TO 9	CRP
	G(K4P1)=CT(4)	CRP
	G(K4P2)=ST(4)	CRP
	DO 8 K=K4P3,K5,2	CRP
	G(K)=G(K-2)*SSMX	CRP
8	G(K+1)=G(K-1)*SSMX	CRP
	IF(K5.EQ.K6) GO TO 9	CRP
	G(K5P1)=CT(5)	CRP
	G(K6)=ST(5)	CRP
	IF(K6.EQ.K7) GO TO 9	CRP
	G(K6P1)=CT(6)	CRP
	G(K7)=ST(6)	CRP
	IF(K7.EQ.K8) GO TO 9	CRP
	G(K7P1)=CT(7)	CRP
	G(K8)=ST(7)	CRP
	IF(K8.EQ.K9) GO TO 9	CRP
	G(K8P1)=CT(8)	CRP
	G(K9)=ST(8)	CRP
9	GAMMA(L)=0.000	CRP
	DO 10 K=1,K9	CRP
10	GAMMA(L)=GAMMA(L)+DKTO(K,L)*G(K)	CRP
100	CONTINUE	CRP
	FCF20=GAMMA(1)*DABS(FFAC)	CRP
	M3000=GAMMA(2)*DABS(MFAC)	CRP
	IF(FFAC.LT.0.000)CALL PERTF(ZT,NLAT,WLONG,FCF20)	CRP
	IF(MFAC.LT.0.000)CALL PERTH(ZT,NLAT,WLONG,M3000)	CRP
	RETURN	CRP

```

      SUBROUTINE PTHP(NLAT,WLONG,A,B)
C      PREDICTED TRUE HEIGHT PROFILE
C      PROGRAMMED FOR D.ODOM BY I.STUHLER
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DOUBLE PRECISION NLAT,M3000,M,J,KK
      LOGICAL SMOOTH
      COMMON/FACCOM/FM,ZZ,KK,P3000
      COMMON/RIIPAR/M3000,FCF20,FCF10,FCEO,HBEF,HPE,HMEP,F1,HMF1P,HMF2
      1,HMF2P,SN,ZT,YR,D,DUM(3),F1FAC,EFAC,H2FAC,
      2 SNSQRT,QRAD,CQ,IO(2),SMOOTH
      DATA RAD/57.2957795130823200/
C      SOLVE FOR ZENITH CORR. ANGLE FOR DAY OF YEAR
      M=23.4500*DSIN(180.00*(D-82.500)/(182.00*RAD))
C      GET F3000 PROPAGATION FREQ FOR F2 LAYER
      F3000=FCF20*M3000
C      CHECK FOR INCORRECT DAY (NEG)
      IF(D.LT.0.000) GO TO 2000
C      IS DAY PAST SPRING
      IF(D.GE.162.500) GO TO 1000
      X=D+365.500
      Y=1.000
      GO TO 1001
C      IS DAY PAST FALL
1000 IF(D.GE.344.500) GO TO 1002
      X=D
      Y=-1.000
      GO TO 1001
C      CHECK FOR INCORRECT DAY (TOO LARGE)
1002 IF(D.GE.366.500) GO TO 2001
      X=D
      Y=1.00
C      SOLVE FOR SOLAR ZENITH ANGLE IN RAD
1001 J=Y*.023500*(64.00/(4.00+DABS((X-344.500)/45.00)**3)-240.00/(15.00
      1 +DABS(X-344.500)))
      IF(ZT.LT.12.00) ZT=-ZT
      Z=DABS(15.00*DABS(ZT-12.00)-J*15.00-WLONG)
      IF(Z.GE.180.00) Z=360.00-Z
      ZSQ=Z*Z
      QSQ=ZSQ*(DCOS(0.600*(NLAT+M)/RAD)**2)+(NLAT-M)**2
1005 Q=DSQRT(QSQ)
      QRAD=Q/RAD
      CQ=DCOS(.93200*QRAD)
C      FUNCTION FOR E-LAYER NIGHT TIME FORMATION
      CCQ=((CQ+1.00)*.500)**2
      SNSQRT=DSQRT(1.00+.00400*SN)
      IF(CQ.LE.0.00) GO TO 1101
C      SOLVE FOR PRED E-LAYER CRITICAL FREQ
C      10.0489=3.17*3.17, .5625=.75*.75
      FCEO=SNSQRT*DSQRT(10.048900*CQ**(2.00/3.77500)+.562500*CCQ**2)
      IF(FCEO.GE.FCF20) FCEO=.7500*SNSQRT*CCQ
      GO TO 1102
1101 FCEO=.7500*SNSQRT*CCQ
C      SOLVE FOR PRED F1-LAYER CRITICAL FREQ
1102 FCF10=1.2600*FCEO+0.500
      IF(FCF10.LT.FCF20*.9900) GO TO 9982
      FCF10=.9900*FCF20
      FCEO=OMAX1((FCF10-.500)/1.2600,1.0-5)

```

```

C SOLVE FOR REF. FREQ. NO. 1 PTH
9982 FK1=FCF20-(FCF20-FCF10)/4.00 PTH
C CALCULATE PRED. SEMITHICKNESS OF F2 LAYER PTH
HPF2=(0.48900*SN+56.000)*H2FAC PTH
C SOLVE FOR REF FREQ. NO. 2 PTH
FK2=FCF20*(1.00-(DSQRT(HPF2)/100.000)) PTH
C SET FM TO GREATER OF TWO REF. FREQ. PTH
IF(FK1.GT.FK2) GO TO 1003 PTH
FM=FK2 PTH
GO TO 1004 PTH
1003 FM=FK1 PTH
C SOLVE FOR VIRTUAL HT. OF F3000 PTH
1004 XX=FM/F3000 PTH
H3000=3100.00*XX**2+70.000 PTH
FC=4.00*FM-3.00*FCF10 PTH
P3000=((FC+3.7800*FCE0+1.500)/(1.2600*FCE0+.500))*DLOG((FC+8.8200 PTH
1 *FCE0+3.500)/(FC-1.2600*FCE0-0.500)) PTH
ZZ=(A-B)*(FC+3.7800*FCE0+1.500)/(8.00*FCE0)*DLOG((FC+7.7800 PTH
* *FCE0+1.500)/(FC-.2200*FCE0+1.500)) PTH
FF=FM/FCF20 PTH
KK=HPF2*FF*DLOG((1.00+FF)/(1.00-FF))/2.000 PTH
C CALCULATE PRED. HT. OF F2 LAYER MAX. PTH
HMF2P=8.00*(H3000-ZZ-B-KK)/P3000+HPF2+A PTH
C CALC. HTS. OF OTHER LAYERS PTH
HMF1P=HMF2P-HPF2 PTH
HMEP=A PTH
HBEP=B PTH
HPF1=HMF1P-HMEP PTH
HPE=A-B PTH
ZT=0ABS(ZT) PTH
FCE0=DMIN1(FCE0*EFAC, (.9900*FCF20-.500)/1.2600) PTH
IF(F1FAC) 1014, 1014, 1015 PTH
1014 FCF10=1.2600*FCE0+.500 PTH
GO TO 1016 PTH
1015 FCF10=FCF10*F1FAC PTH
1016 IF(SMOOTH) FCF10=FCF10/.86602540378443900 PTH
FCF10=DMIN1(FCF10, .9900*FCF20) PTH
RETURN PTH
2000 WRITE(6,4)0 PTH
4 FORMAT(4H 0 =D13.5,12H IS NEGATIVE) PTH
STOP PTH
2001 WRITE(6,5)0 PTH
5 FORMAT(4H 0 =D13.5,22H IS GREATER THAN 366.5) PTH
STOP PTH
END PTH

```



```

      SUBROUTINE NFROMR(RFEC,PLASD)
C
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DOUBLE PRECISION K,J,M3000
      LOGICAL SMOOTH
      COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAЕ,HME,HAF1,HMF1,HAF2,HMF2,
      1DUM(10),SNSQRT,QRAD,CQ,IO,IA,SMOOTH
C  HEIGHT ABOVE GROUND OF REF. PT.
      OH=RFEC-6370.00
C  NO - IS PCINT OF INTEREST ABOVE E LAYER MAX
      IF(OH.GT.HME) GO TO 201
      IF(ID.EQ.1) GO TO 2001
C  IS PT. OF INTEREST BELOW E LAYER
      IF((HME-OH).GE.HAE) GO TO 300
C  NO - SOLVE FOR E LAYER PLASMA DENSITY
      F02=FCE*FCE*(1.00-((HME-OH)/HAE)**2)
      GO TO 202
C  E LAYER WITH D LAYER TAIL
2001 ZP=2.00*(HME-OH)/HAE
      K=1.500*DSQRT(1.700/(1.700+ZP))
      J=1.00+(ZP-1.00)*DABS(ZP-1.00)/10.00
      J=J/(1.00-.100/(1.00+ZP)**2)
      ZPP=2.00
      IF(ZP.GT.0.00) ZPP=2.00-DLOG(1.00+1.7200*ZP**K)
      IF(ZPP.LE.0.00) GO TO 300
      ZPP=2.00-ZPP**J
      F02=FCE*FCE*(1.00-ZPP*ZPP/4.00)
      GO TO 202
C  SOLVE FOR REF. HTS. 1 THRU 3
201 HS2=HMF2-HAF2*DSQRT(1.00-(FCF1/FCF2)**2)
      HS1=HMF1-HAF1*DSQRT(1.00-(FCE/FCF1)**2)
      HT2=(HS2+HMF1)/2.00
C  IS PT. OF INTEREST ABOVE REF PT 3
      IF(OH.GT.HT2) GO TO 203
C  NO- SOLVE FOR F1 LAYER PLASMA DENSITY
      BIGK1=(HS1-HME+HS2-HMF1)/(2.00*(FCF1-FCE))
      BIGK3=HAF1/FCF1
      BIGK2=HMF1-(FCF1*(HS1-HME)+FCE*(HS2-HMF1))/(2.00*(FCF1-FCE))
      BIGA=BIGK1**2+BIGK3**2
      BIGB=2.00*BIGK1*(BIGK2-OH)
      BIGC=OH**2-2.00*OH*BIGK2+BIGK2**2-HAF1**2
      FO=(-BIGB+DSQRT(BIGB**2-4.00*BIGA*BIGC))/(2.00*BIGA)
      IF(FO.LT.FCE) FO=FCE
      F02=FO*FO
      GO TO 202
C  SOLVE FOR DENSITY ABOVE F2 LAYER MAX
211 OHH=(OH-HMF2)/OH
      Z=(OH-HMF2)/HAF2*2.00
      F02=FCF2**2*DEXP(1.00-Z-DEXP(-Z))+(0.500+FCF2/10.000)*OHH*HMF2/OH
      F02=DMIN1(F02,FCF2**2)
      GO TO 202
C  IS POINT OF INTEREST ABOVE F2-LAYER MAX
203 IF(OH.GT.HMF2) GO TO 211
C  NO-SOLVE FOR F2-LAYER PLASMA DENSITY
      BIGK1=(HS2-HMF1)/(2.00*(FCF2-FCF1))
      BIGK3=HAF2/FCF2
      BIGK2=HMF2-FCF2*BIGK1

```

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	BIGA=BIGK1**2+BIGK3**2	NFR
	BIGB=2.00*BIGK1*(BIGK2-OH)	NFR
	BIGC=OH**2-2.00*OH*BIGK2+BIGK2**2-HAF2**2	NFR
	F0=(-BIGB+DSQRT(BIGB**2-4.00*BIGA*BIGC))/(2.00*BIGA)	NFR
	F02=F0*F0	NFR
202	PLASD=F02*12400.00	NFR
	IF(ID.EQ.1) GO TO 301	NFR
	RETURN	NFR
300	PLASD=0.00	NFR
	IF(ID.EQ.0) RETURN	NFR
301	CQ=DCOS(QRAD*.8500)	NFR
	IF(CQ.GT.0.000) GO TO 302	NFR
	CQ=0.00	NFR
	RETURN	NFR
302	CQ=CQ** (0.2500)	NFR
303	PLASD=PLASD+SNSQRT*SNSQRT*CQ*1.02/(1.00+81.00*((65.00-OH)/HAE)**4)	NFR
	RETURN	NFR
	END	NFR

```

      SUBROUTINE DFP(NLATA,WLONGA,NLATB,WLONGB,DIST)
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DOUBLE PRECISION NLATA,NLATB
      DATA RAD/57.2957795130823200/
      DACOS(DUMMY)=DATAN2(DSQRT(1.000-DUMMY*DUMMY),DUMMY)
C   SHIFT INPUT LAT. BY ONE QUADRANT
      PPA=90.000-NLATA
      PPB=90.000-NLATB
      GGH=WLONGA
      G GK=WLONGB
C   FIND SMALLEST ANGULAR DIFF. BETWEEN A AND B
      HHGK=GGH-GGK
      ABHHGK=DABS(HHGK)
      HHK=ABHHGK
      IF(HHK.GT.180.00) HHK=360.00-HHK
C   SOLVE FOR BEARING FROM A TO B
      RAAPB=HHK/RAD
      CSAAPB=DCOS(RAAPB)
      RPPA=PPA/RAD
      SINPPA=DSIN(RPPA)
      COSPPA=DCOS(RPPA)
      RPPB=PPB/RAD
      SINPPB=DSIN(RPPB)
      COSPPB=DCOS(RPPB)
      COSAAB=COSPPA*COSPPB+SINPPA*SINPPB*CSAAPB
      RAAB=DACOS(COSAAB)
C   SOLVE FOR GREAT CIRCLE DISTANCE BETWEEN A AND B
      DIST=6370.000*RAAB
      RETURN
      END

```

```

SUBROUTINE MMDIP(NLAT,WLONG,SSMX)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
C COMPUTE MAGNETIC FIELD COMPONENTS MAGNETIC DIP AND MODIFIED MAGNETIC
C DIP
DOUBLE PRECISION NLAT
DIMENSION P(7,7),DP(7,7),CP(7),AOR(7),SP(7)
DIMENSION CT(7,7),H(7,7),G(7,7)
DATA P,DP,SP/1.000,104*0.000/,CP/1.000,6*0.000/
DATA RD/57.2957795130823200 /,HC/6371.203/
DATA CT/2*0.00,.3333333300,.26666666700,.2571428600,
1 .2539682500,.2525252500,3*0.00,.200,.2285714200,.2380952300,
2 .2424242400,4*0.00,.1428571400,.1904761900,.2121212100,
3 5*0.00,.1111111100,.1616161600,6*0.00,.0909090900,14*0.00/
DATA G/0.00,.30411200,.02403500,-.03151800,-.04179400,
1 .01625600,-.01952300,0.00,.02147400,-.05125300,
2 .06213000,-.04529800,-.03440700,-.00485300,2*0.00,
3 -.01338100,-.02489800,-.02179500,-.01944700,.00321200,
4 3*0.00,-.00649600,.00700800,-.05060800,.02141300,
5 4*0.00,-.00204400,.00277500,.00105100,5*0.00,.00069700,
6 .00022700,6*0.00,.00111500/
DATA H/8*0.00,-.05798900,.03312400,.01487000,-.01182500,
1 -.00079600,-.00575800,2*0.00,-.00157900,-.00407500,
2 .01000600,-.002000,-.00873500,3*0.00,.0002100,.0004300,
3 .00459700,-.00340600,4*0.00,.00138500,.00242100,
4 -.00011800,5*0.00,-.00121800,-.00111600,6*0.00,
5 -.00032500/
P1=NLAT
P2=360.000-(WLONG)
IF(P1-89.900)2,4,1
1 P1=89.900
P2=0.00
GO TO 4
2 IF(P1+89.900)3,4,4
3 P1=-89.900
P2=0.00
4 PHI=P2/RD
AR=HC/(HC+3.D5)
C=DSIN(P1/RD)
S=DSQRT(1.-C**2)
SP(2)=DSIN(PHI)
CP(2)=DCOS(PHI)
AOR(1)=AR**2
AOR(2)=AR**3
DO 5 M=3,7
SP(M)=SP(2)*CP(M-1)+CP(2)*SP(M-1)
CP(M)=CP(2)*CP(M-1)-SP(2)*SP(M-1)
5 AOR(M)=AR*AOR(M-1)
BV=0.00
BN=0.00
BPHI=0.00
DO 6 N=2,7
FN=DBLE(FLOAT(N))
SUMR=0.00
SUMT=0.00
SUMP=0.00
DO 7 M=1,N
IF(N-M)8,9,8

```

```

9      P(N,N)=S*P(N-1,N-1)                                DMH
      DP(N,N)=S*DP(N-1,N-1)+C*P(N-1,N-1)                  DMH
      GO TO 10                                              DMH
8      P(N,M)=C*P(N-1,M)-CT(N,M)*P(N-2,M)                 DMH
      DP(N,M)=C*DP(N-1,M)-S*P(N-1,M)-CT(N,M)*DP(N-2,M)    DMH
10     FM=DOUBLE(FLOAT(M-1))                                DMH
      TS=G(N,M)*CP(M)+H(N,M)*SP(M)                        DMH
      SUMR=SUMP+P(N,M)*TS                                  DMH
      SUMT=SUMT+DP(N,M)*TS                                  DMH
7      SUMP=SUMP+FM*P(N,M)*(-G(N,M)*SP(M)+H(N,M)*CP(M))   DMH
      BV=BV+AOR(N)*FN*SUMR                                  DMH
      BN=BN-AOR(N)*SUMT                                      DMH
6      BPHI=BPHI-AOR(N)*SUMP                                DMH
      COSLAM=DCOS((NLAT)/RD)                                DMH
      COM1=-BV                                              DMH
      COM2=BN                                               DMH
      COM3=-BPHI/S                                          DMH
      TMP=COM2**2+COM3**2                                    DMH
      BIGI=DATAN(-COM1/DSQRT(TMP))                          DMH
      SSMX=(BIGI/DSQRT(BIGI**2+COSLAM))                     DMH
C      NEXT CARD DELETED DSINCE SMX NOT USED BY CRPL2      DMH
C      SMX=DASIN(SSMX)                                       DMH
      RETURN                                                DMH
      END                                                    DMH

```

ROUTINE PERT.F

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SUBROUTINE PERTF(T,NL,WL,FCF20)	PER
IMPLICIT DOUBLE PRECISION (A-H,O-Z)	PER
DOUBLE PRECISION NLREF,MR,MZ,MD,NL	PER
COMMON/PERTC/NLREF,WLREF,FR,FD,MR,MD,FZ,MZ,DUT,DW,X,GAMMA,AZM,	PER
1 DFAC,DNAC,AZREF	PER
RTD=57.2957795130823200	PER
CALL DFP3(NLREF,WLREF,NL,WL,DIST,AZ)	PER
AZ=AZ-AZREF	PER
STHINV=1.000/DABS(DSIN((AZM-(90.00+GAMMA))/RTD))	PER
Y=DUT*3600.00*X*STHINV	PER
W=DW*STHINV	PER
SD=DSIN((DIST+Y)/W*360.00/RTD)	PER
FCF20=FCF20*(1.00+FZ*SD)*(1.00+FR*DIST/MD)*(1.00+AZ*DFAC)	PER
FCF20=AMAX1(.5100,FCF20)	PER
RETURN	PER
ENTRY PERTM(T,NL,WL,FCF20)	PER
FCF20=FCF20*(1.00+MZ*SD)*(1.00+MR*DIST/MD)*(1.00+AZ*DNAC)	PER
FCF20=AMAX1(1.00,FCF20)	PER
RETURN	PER
END	PER

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```

SUBROUTINE FACTO(NLREF,HLREF,FCF2R,HMINR,ZTREF)
IMPLICIT DOUBLE PRECISION(A-H,O-Z)
DOUBLE PRECISION KK,M3000P,M3000R,MFAC,MM,NLREF,K1
COMMON/FACCOM/FH,ZZ,KK,P3000
COMMON/RIIPAR/M3000P,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HPF2,
1 HMF2,SNS(5),MFAC,F2FAC,DUM(6),IDUM(3)
DATA RTD/57.2957795130823200/
F2FAC=1.00
MFAC=1.00
IF(FCF2R.EQ.0.00) RETURN
ZTS=SNS(2)
SNS(2)=ZTREF
CALL CRPL2(NLREF,HLREF)
F2FAC=DABS(FCF2R/FCF2)
IF(HMINR.EQ.0.00) GO TO 10
CALL RIIP(6370.00,NLREF/RTD,HLREF/RTD,PLASD)
P1=(FCF2+3.7800*FCE+1.500)/FCF1*DLOG((FCF2+8.8200*FCE+3.500)/
1 (FCF2-FCF1))
MM=HAE/8.00
Z1=MM*(FCF2+3.7800*FCE+1.500)/FCE*DLOG((FCF2+7.7800*FCE+1.500)/
1 (FCF2-.2200*FCE+1.500))
FFM=FCF1+(FCF2-FCF1)/4.00
FF1=FFM/FCF2
K1=50.00*FF1*DLOG((1.00+FF1)/(1.00-FF1))
H3000=P3000/P1*(DABS(HMINR)-Z1-HBE-HPF2*K1/100.00)+ZZ+HBE+KK
M3000R=(FH/FCF2)*DSORT(3100.00/(H3000-70.00))
MFAC=DSIGN(M3000R/M3000P,HMINR)
F2FAC=DSIGN(F2FAC,FCF2R)
10 SNS(2)=ZTS
RETURN
END

```

## Appendix B

### Block Diagram and Flow Chart for WIMP Ray-Tracing Program TRISL

Explanation:

#### BI. TRISL BLOCK DIAGRAM

This presentation shows the general communication network among the various functional processes of TRISL, and illustrates the iterative complications inherent in the program. The function of the various blocks is generally described as follows:

- BLOCK I: Initialization Procedures.
- BLOCK II: E-layer refraction upwards.
- BLOCK III:  $F_1$ -layer refraction upwards.
- BLOCK IV: Reflection layer initialization.
- BLOCK V: Tilt calculation and consistency checks.
- BLOCK VI:  $F_1$ -layer refraction downwards.
- BLOCK VII: E-layer refraction downwards.
- BLOCK VIII: Error checks.
- BLOCK IX: Iterate reflection and tilt.
- BLOCK X: Traffic control.
- BLOCK XI: Normal Terminal calculations.
- BLOCK XII: ERROR exits.



## B2. DETAILED FLOW CHARTS

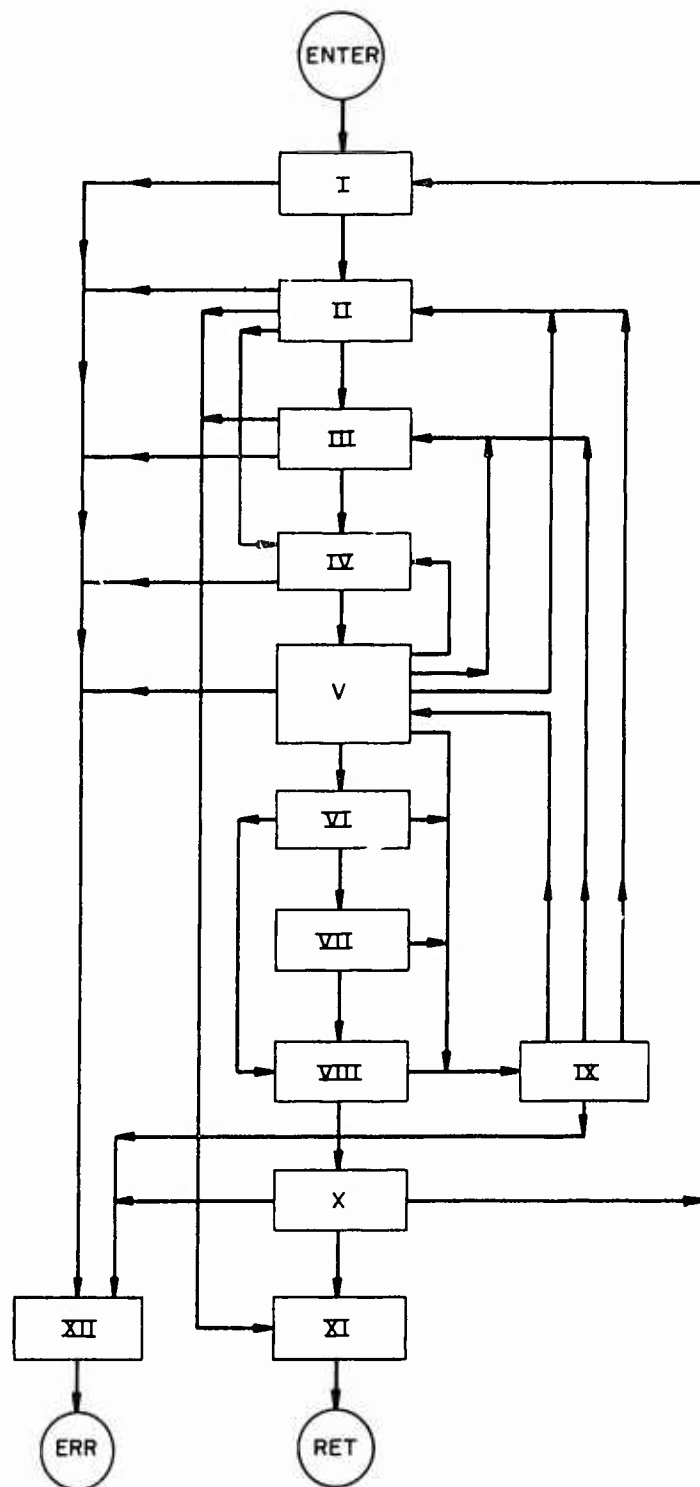
Detailed flow charts are presented for each block. Most line members of TRISL are accounted for except when so doing unduly complicates comprehension of the process.

## B3. FLOW CHART SYMBOLS AND CONVENTIONS

- (a) Process entry/exit point.
- (b) Processing statements.
- (c) Decision trees, two or three way branches.
- (d) External procedures.
- (e) Numbers in the form Snnn refer to statement numbers in the program.
- (f) Numbers in the form nnn refer to line numbers of the program listing.
- (g) Entry points to a block are labelled generally with block designation state-ment number and line number specifying the source.
- (h) Exit points from a block are generally labelled by block designation, state-ment number, and line number specifying the destination.
- (i) Error exits are labelled by an error number and the error condition detected.
- (j) Exits from the bottom generally enter the next block at the top.
- (k) External call names and calling line numbers are contained within the external procedure symbols.

## B4. PROGRAM LISTING

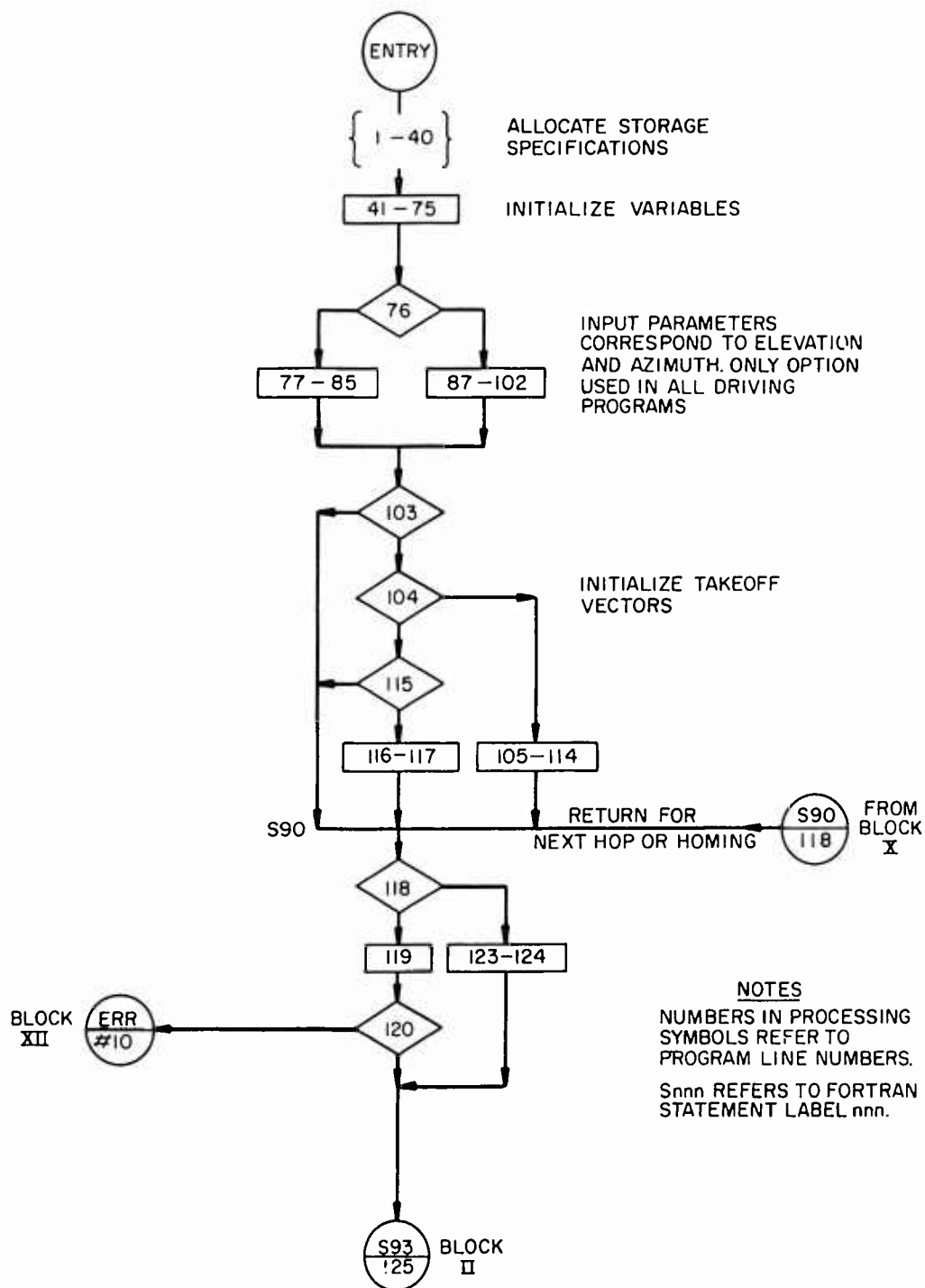
Listings are included for TRISL together with its externals.



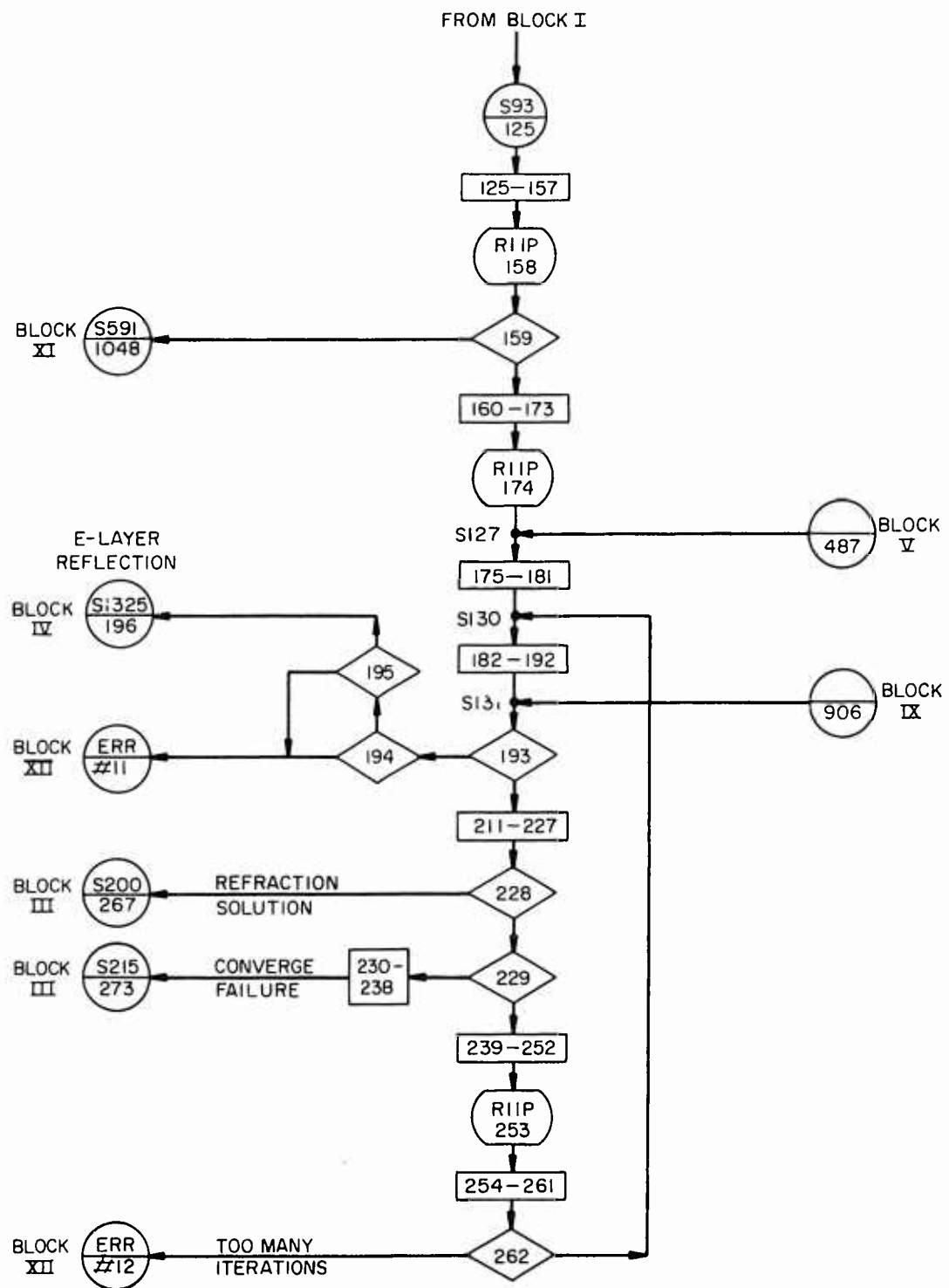
TRISL Block Diagram

TRISL: Block I, Argument List

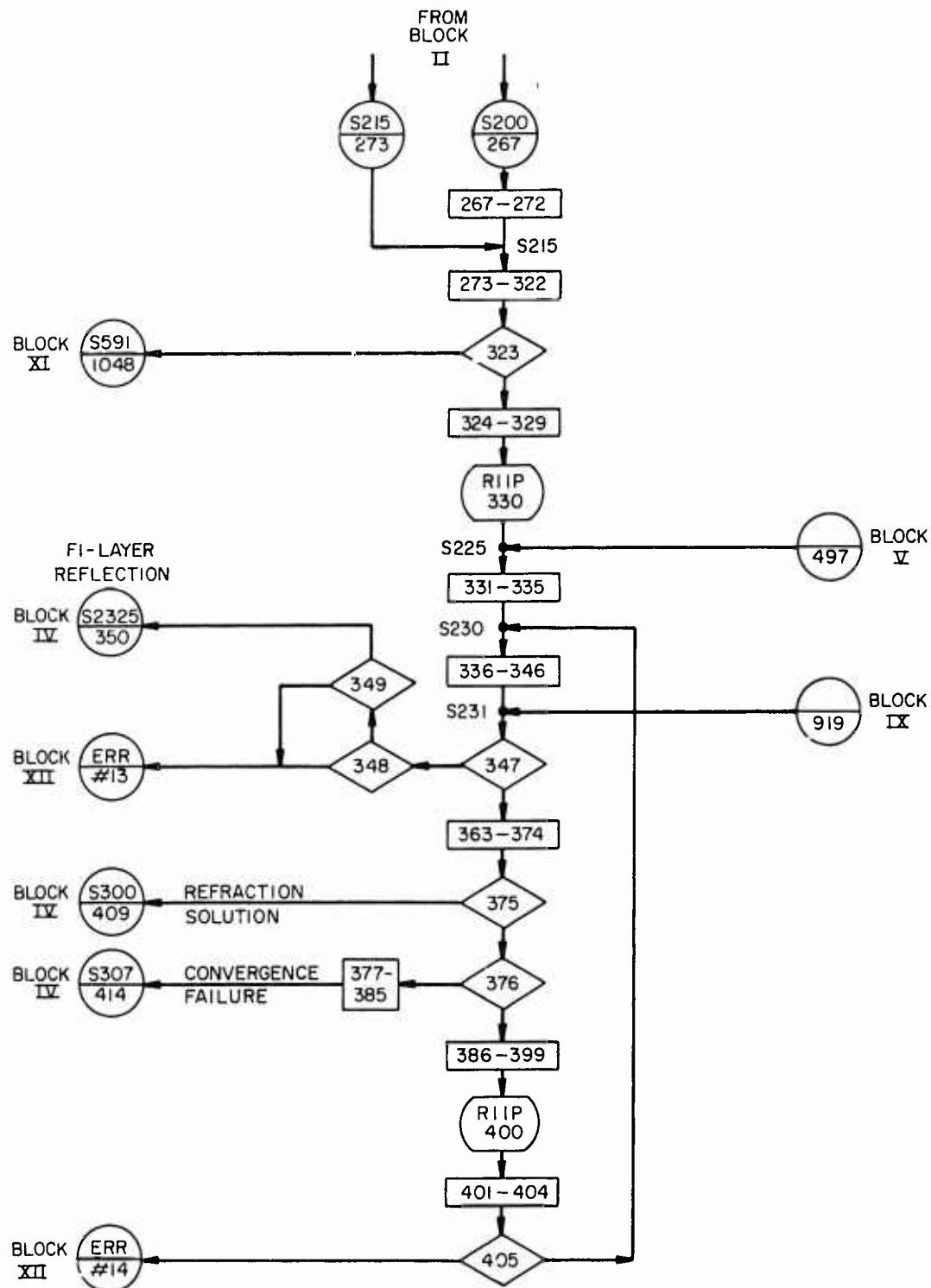
Element	I/D	Mnemonic	Type	Definition
1	I	MAI	Double	Geocentric Distance, Initial Point
2	I	NLAI	Double	North Latitude, Initial Point
3	I	WLAI	Double	West Longitude, Initial Point
4	I	NLAZ	Double	Takeoff Bearing (all calls) or Target North Latitude
5	I	WLAZ	Double	Takeoff Elevation (all calls) or Target West Longitude
6	I	MAZ	Double	Less than 6000 km (all calls) or Target Geocentric Distance
7	I	FREQ	Double	Frequency
8	I	MODE	Integer	MODE  = Number of hops
9	I	RTARG	Double	= 6370 km, (all calls)
10	O	RS 2	Double	Geocentric Distance, End Point
11	O	NLTARG	Double	North Latitude, End Point
12	O	WLTARG	Double	West Longitude, End Point
13	O	PPTOT	Double	Phase Path Length
14	O	GPTOT	Double	Group Path Length
15	O	AZF	Double	Final to Initial Azimuth
16	O	ELF	Double	End Point Elevation
17	O	SRANGE	Double	Final-Initial Straight Line Distance
18	O	ELSR	Double	Takeoff Elevation
19	O	DIST	Double	Final-Initial Great Circle Ground Range
20	O	BEAR	Double	Initial to Final Azimuth
21	O	IGOBAK	Integer	Error Flag 8 = 0 No Error = 1 Fatal Error = 2 Penetrate



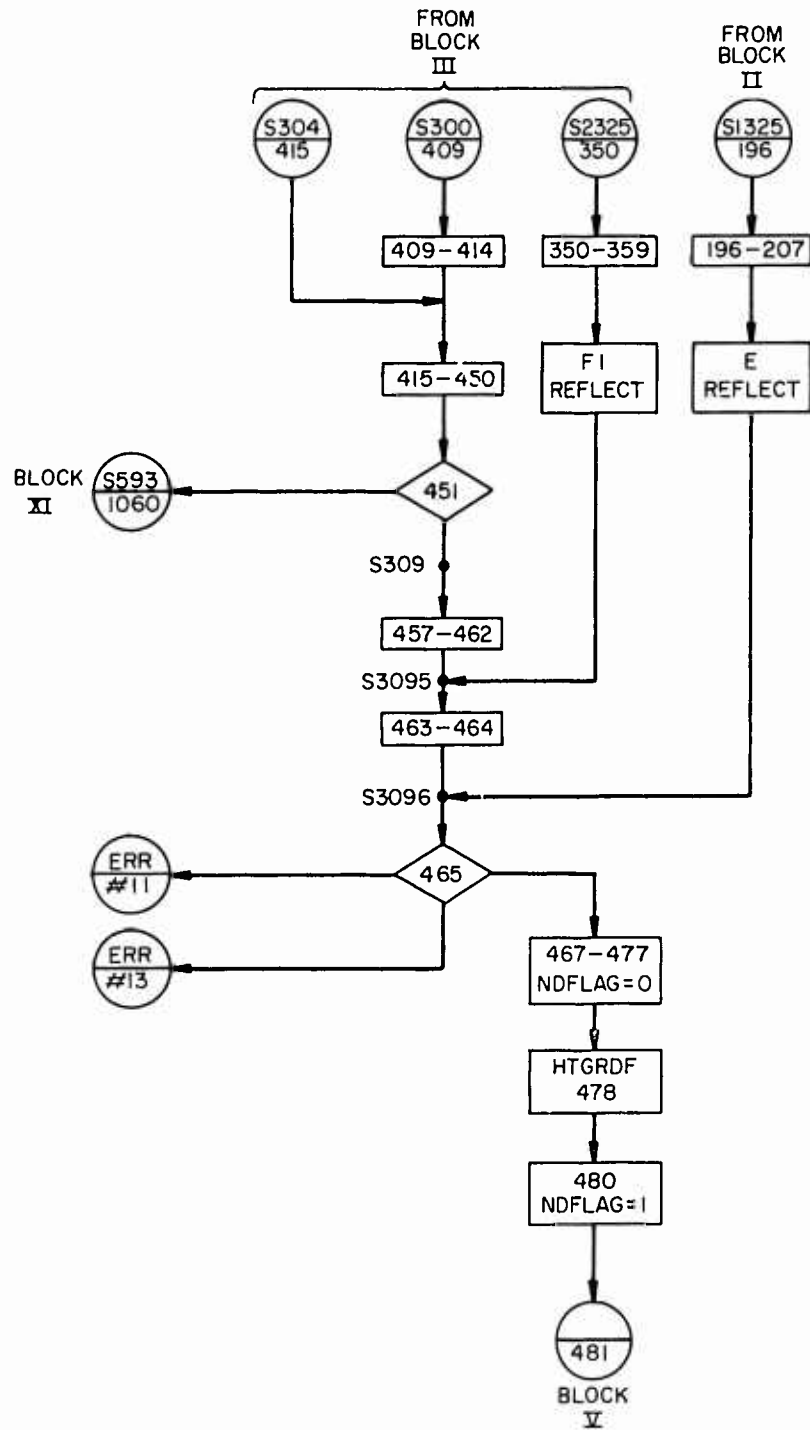
Block I, Initialization Procedures



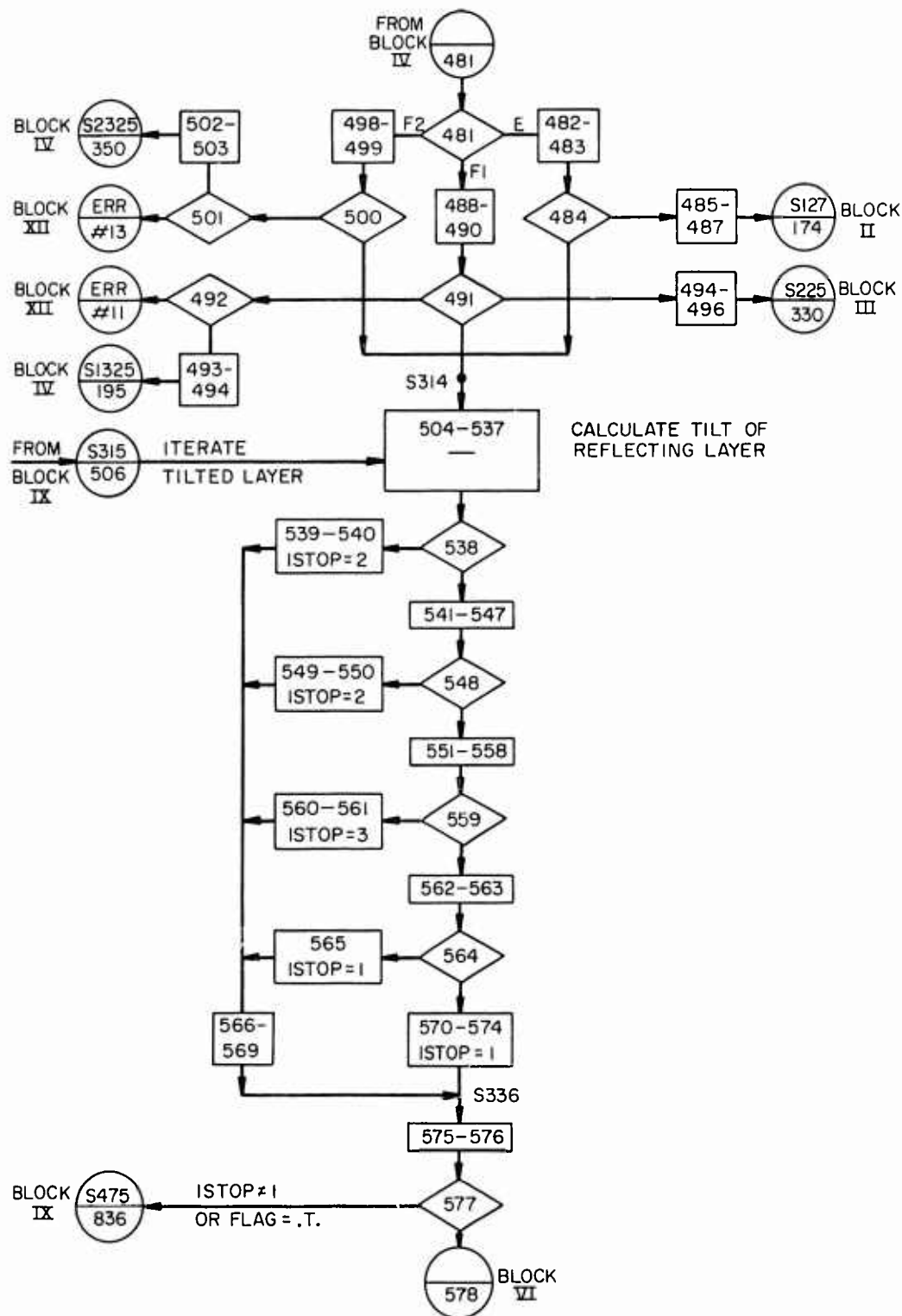
Block II, E-Layer Refraction Upwards



Block III,  $F_1$ -Layer Refraction Upwards

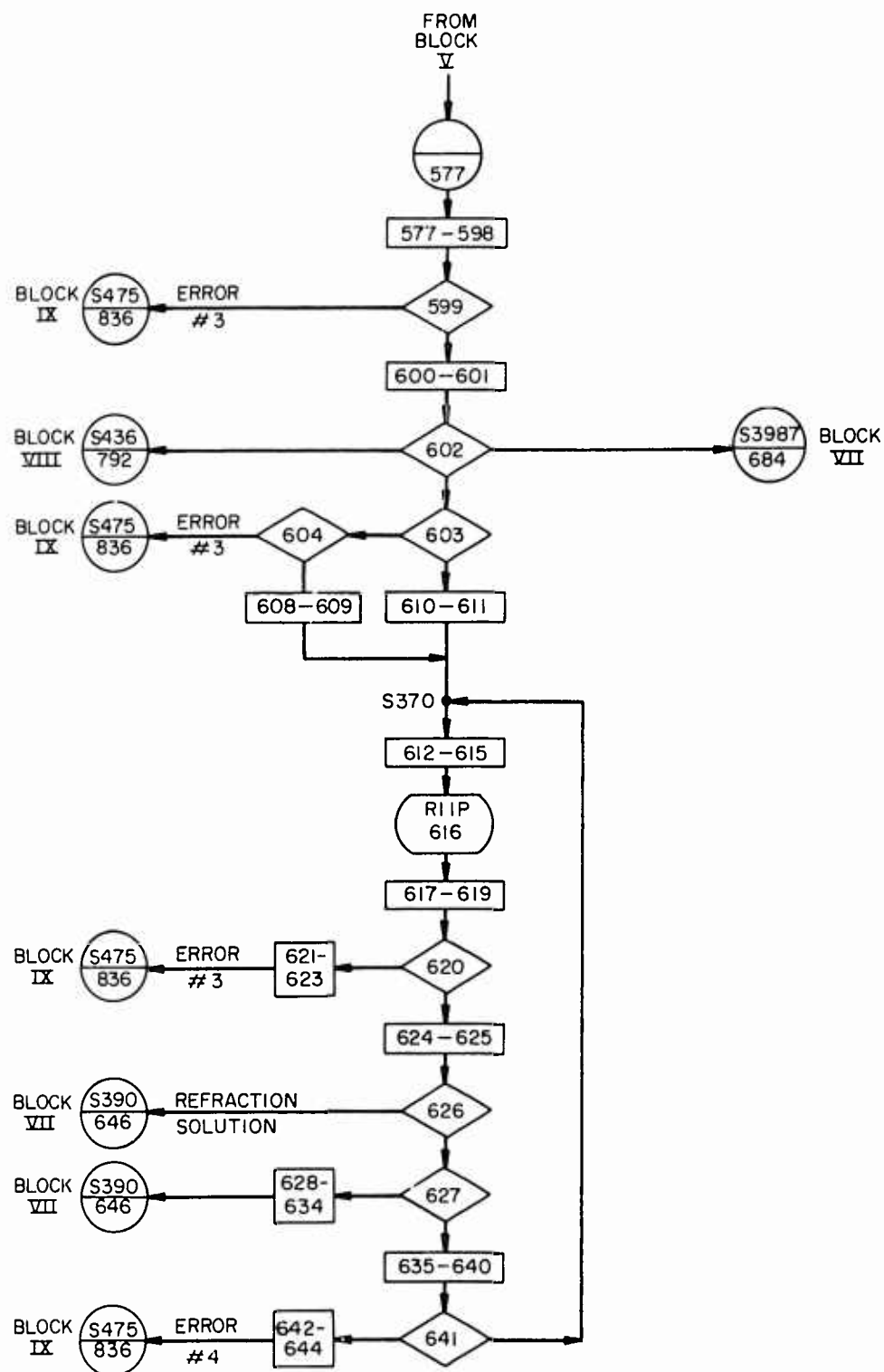


Block IV, Reflection Layer Initialization

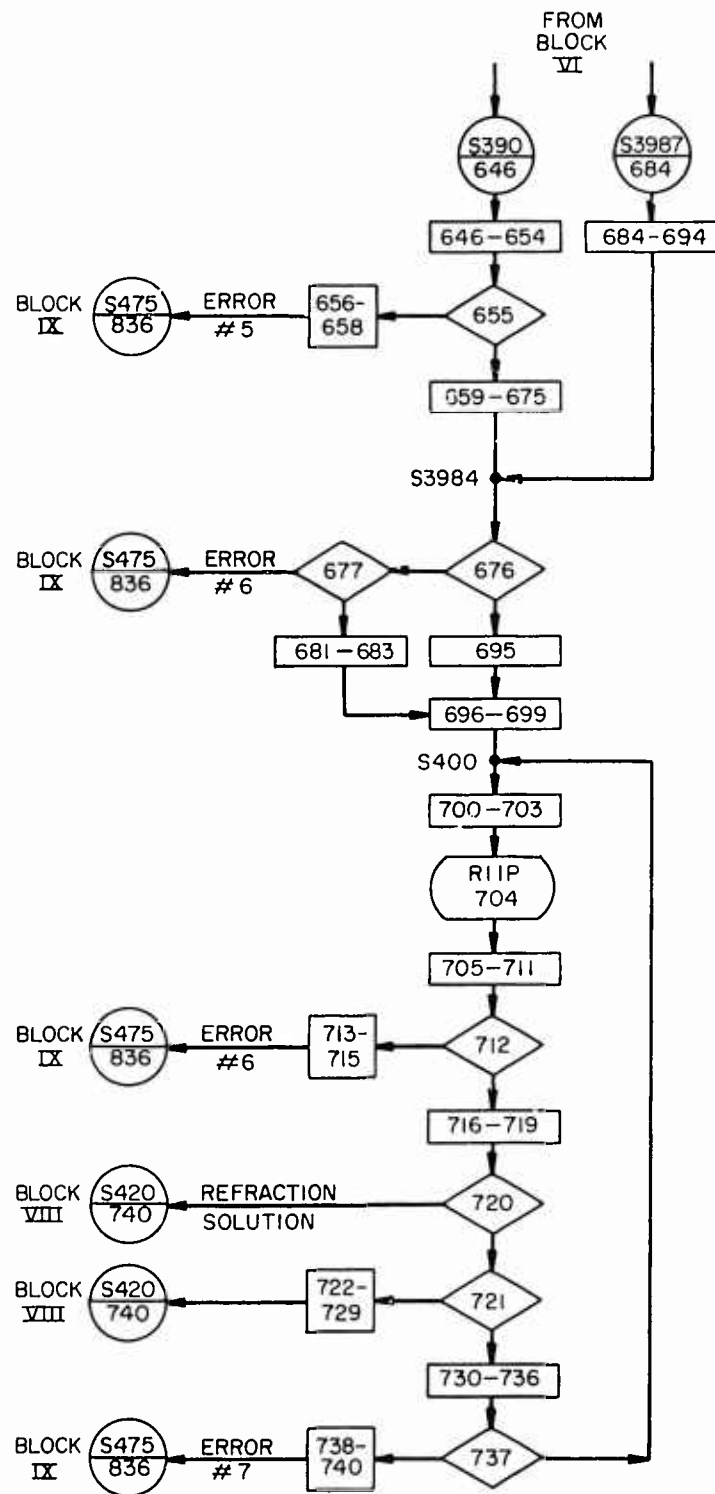


Block V, Tilt Calculation and Consistency Checks

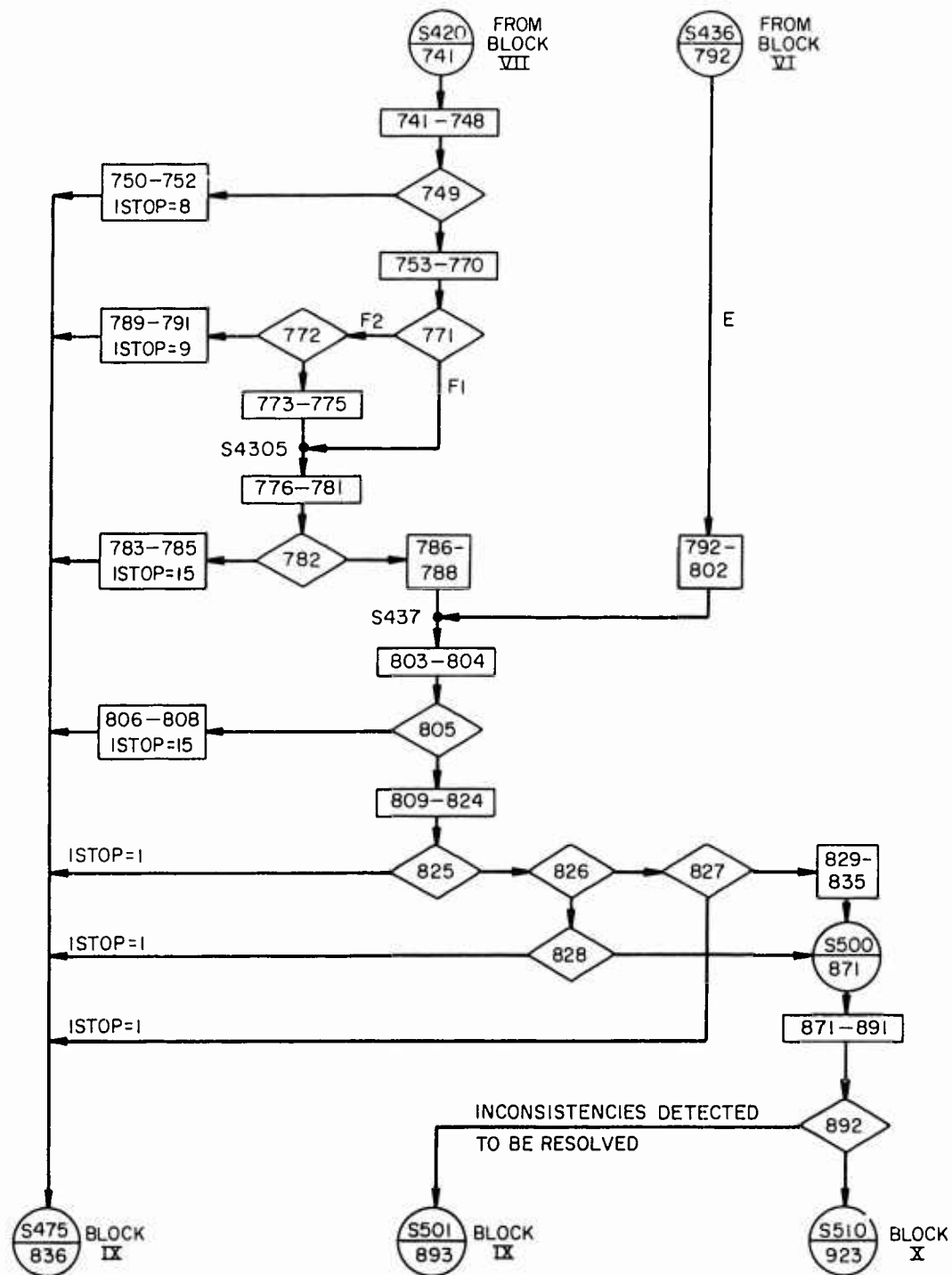




Block VI,  $F_1$ -Layer Refraction Downwards



Block VII, E-Layer Refraction Downwards

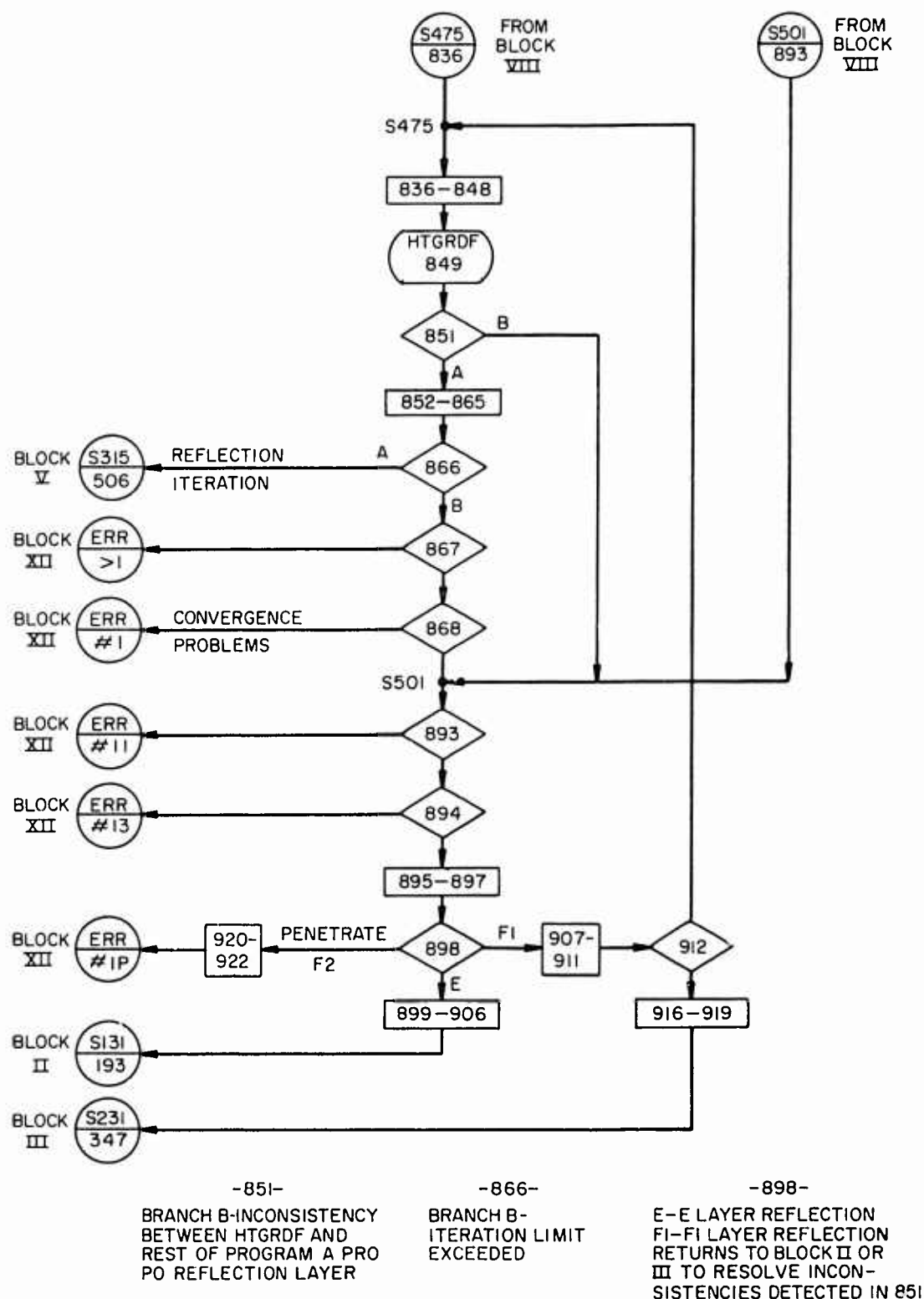


#### NOTES

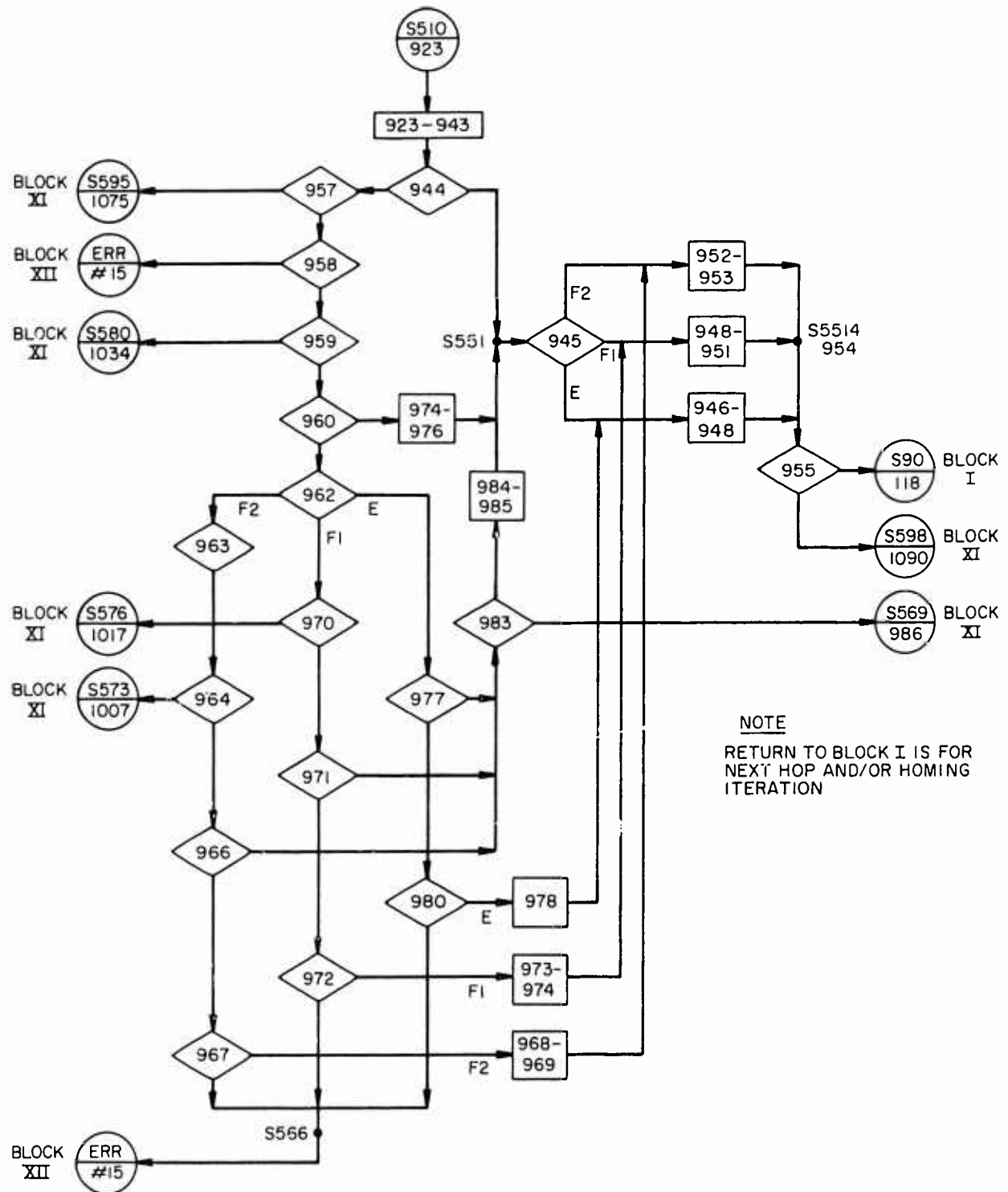
BLOCK X EXIT IS DESIRED CONVERGENT SOLUTION TO TILTED LAYER ITERATION

THE ISTOP=1 EXITS TO S475 ARE NORMAL. THE OTHER ERROR CONDITIONS MAY BE CORRECTED IN SUCCEEDING ITERATIONS

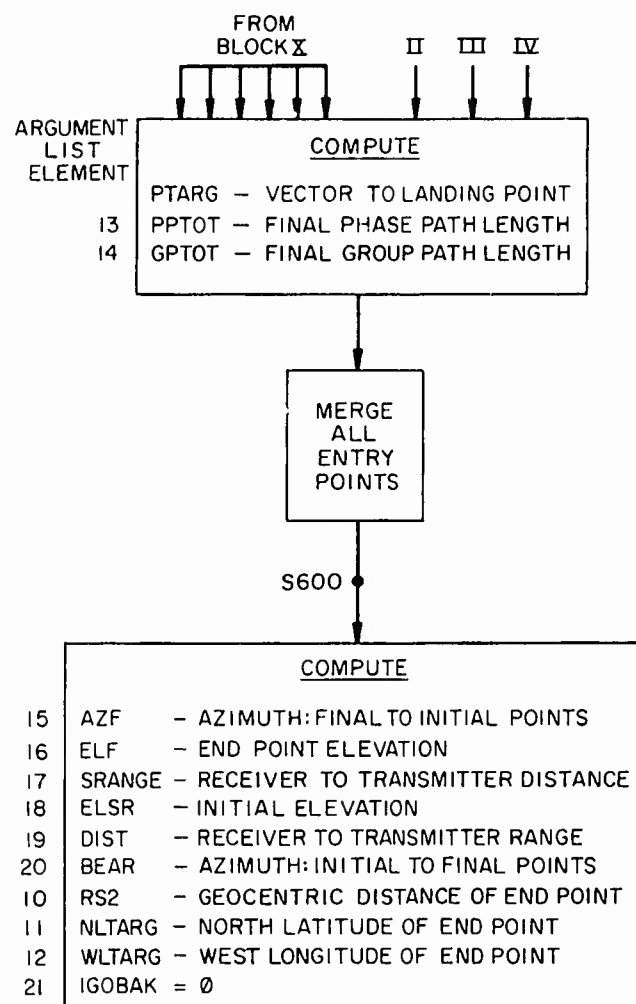
Block VIII, Error Checks



Block IX, Iterate Reflection and Tilt



Block X, Traffic Control



Block XI, Normal Terminal Calculations

```

SUBROUTINE TRISL(MA1,NLA1,WLA1,NLA2,WLA2,MA2,FREQ,MODE,RTARG,RS2, TR2
*NLTARG,HLTARG,PPTOT,GPTOT,AZF,ELF,SRANGE,ELSR,DIST,BEAR,IGOBAK) TR2
IMPLICIT DOUBLE PRECISION (A-H,O-Z) TR2
LOGICAL HITS,FLAG,SEARCH,ASC,FLAG2,FLAG3,NOELAY,INCHOP,LP(6),NIP TR2
LOGICAL GPONLY TR2
DOUBLE PRECISION MESSPR TR2
DOUBLE PRECISION NLA1,MA1,NLA2,MA2,NLTARG,MAG,MA1B1,MB1,NLC1,NL4, TR2
1MRX1SQ,NLC2,MR3,NL8,NLC3,MN1,MA2C2,MC2,MA3C3,MC3,NLD,MRM1,MRM2, TR2
2MRY1SQ,MC4SQ,NLE,MRM3,MRM4,MC5SQ,NLW2,KP,L,N1,M,KPPP,LOC, TR2
3MAGVEC,NORTH(3),ME,MN,NORTH1(3),EAST1(3),MR2,MC1PSQ,M3000 TR2
REAL OUT2 TR2
DIMENSION S1(3),A1(3),B1(3),A11(3),EAST(3),MESSPR(15), TR2
* XI(3),KP(3),L(3,3),P1P(3),PC2(3),P8(3),R3(3),PC3(3),P10(3),C TR2
*2(3),PR1(3),N1(3),P0(3),A2(3),M(3,3),C3(3),A3(3),PHI(3),KPPP(3),P( TR2
*3,3),PD(3),PE(3),PQ(3),PW2(3),W2(3),PTARG(3), RN1(3),R2(3 TR2
*),PC1(3),P4(3) TR2
COMMON/FLIMSY/DIST1,ICNPRB /GPFLAG/GPONLY,IWRITE TR2
COMMON/CPREV/PQ,P,RT1,C52PPP,C53PPP,MRM1,CBETM1,MRM4,RY, TR2
2 DPP1P,MC5SQ,RM1,YY2PPP,ZY2PPP,H1,MC4SQ,MRY1SQ,YY1PPP, TR2
2 ZY1PPP,C42PPP,C43PPP,YS3PPP,ZS3PPP,C32PPP,RTM1,DNDNL, TR2
3 DNDWL,D,GNU,PP2,PPEF1D,CBETM2,HE,PPF2,RV,HF1,PP2A,DPP2P, TR2
4 MB1,SBET1,GPF2,GPEF1D,DGP2P,DGP1P, TR2
5 F1,PREV(56),HITS,INCHOP,FLAG,FLAG2,FLAG3,NOELAY,LP TR2
COMMON/VECTRS/LOC(3,8),VEC(3,6),IREFL TR2
COMMON/NIPRIP/NIP TR2
*/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2,DUM(13 TR2
*),ID(3)/RTCOM/COSB0,NUSE TR2
COMMON/REMHEN/INUSE,NNUSE(20),FCREF(20) TR2
DATA R,EPS1,EPS2,EPS3,EPS4,EPS5/6670.00,5*1.00/ TR2
DATA PI,RTD,DIR,R0/3.14159265358979300,57.2957795130823200, TR2
*.0174532925199433000,6370.00/ TR2
DATA LIMEA,LIMF1A,LIMF1D,LIMEO,LIMF2/5*15/ TR2
DATA MESSPR/7HF2 ITER,8HBIG TILT,8HBIG TILT,9HF1-D ITER, TR2
1 9HF1-D REFL,7HF1 MISS,8HE-D ITER,8HE-D REFL,6HE MISS, TR2
2 8HI-I REFL,9HE-F1 DUCT,8HE-A ITER,10HF1-F2 DUCT, TR2
3 9HF1-A ITER,9HMISS TARG/ TR2
WLOH(ARG1,ARG2)=DSIGN(PI,ARG1)+PI-DATAN2(ARG1,ARG2) TR2
DACOS(ARG1)=DATAN2(DSQRT(1.00-ARG1**2),ARG1) TR2
DASIN(ARG1)=DATAN2(ARG1,DSQRT(1.00-ARG1**2)) TR2
INCHOP=.TRUE. TR2
HITS=.TRUE. TR2
ASC=MODE.EQ.0 TR2
SEARCH=ASC TR2
PP0=0.00 TR2
PPEF1A=0.00 TR2
DPP1=0.00 TR2
PP2A=0.00 TR2
PPF2=0.00 TR2
PP2=0.00 TR2
PPEF1D=0.00 TR2
DPP2P=0.00 TR2
PP0P=0.00 TR2
PPTOT=0.00 TR2
GPTOT=0.00 TR2
GPEF1A=0.00 TR2
DGP1=0.00 TR2
DGP2=0.00 TR2

```

```

GPEF1A=0.00
GPF2=0.00
GPEF1D=0.00
DGP2P=0.00
DGP1F=0.00
XCHPRB=0
INUSE=0
IGOBK=0
IHOPS=0
RS2=RTARG
CN=DCOS(NLA1*DTR)
SN=DSIN(NLA1*DTR)
CW=DCOS(WLA1*DTR)
SW=DSIN(WLA1*DTR)
A1(1)=CN*CW
A1(2)=-CN*SW
A1(3)=SN
IF(MA2.LT.6000.00) GO TO 50
CN=DCOS(NLA2*DTR)
DO 45 I=1,3
A11(I)=MA1*A1(I)
45 A1(I)=A11(I)
B1(1)=MA2*DCOS(WLA2*DTR)*CN-A1(1)
B1(2)=-MA2*DSIN(WLA2*DTR)*CN-A1(2)
B1(3)=MA2*DSIN(NLA2*DTR)-A1(3)
MB1=MAG(B1)
DTA1B1=DOT(A1,B1)
GO TO 60
C WHEN MA2 IS INPUTTED AS A NUMBER LESS THAN 6000, NLA2 IS ASSUMED
C TO BE THE BEARING,AND WLA2 IS ASSUMED TO BE THE TAKE-OFF ANGLE
50 EAST1(1)=SW
EAST1(2)=CW
EAST1(3)=0.00
CALL CROSS(A1,EAST1,NORTH1)
CAZ=DCOS(NLA2*DTR)
SAZ=DSIN(NLA2*DTR)
CEL=DCOS(WLA2*DTR)
SEL=DSIN(WLA2*DTR)
DO 55 I=1,3
B1(I)=CEL*(CAZ*NORTH1(I)+SAZ*EAST1(I))+SEL*A1(I)
A11(I)=MA1*A1(I)
55 A1(I)=A11(I)
MB1=1.00
DTA1B1=SEL*MA1
60 IF(DABS(MA1-R0).LE.1.0-5) GO TO 90
IF(DASIN(R0/MA1)-DACOS(-DTA1B1/(MA1*MB1)))88,88,80
80 T1=(-DTA1B1-DSQRT(DTA1B1**2-DOT(B1,B1)*(DOT(A1,A1)-R0**2)))
*/DOT(B1,B1)
DO 85 J=1,3
85 A1(J)=B1(J)*T1+A1(J)
A=-2.00*DOT(A1,B1)/DOT(A1,A1)
DO 87 J=1,3
87 B1(J)=B1(J)+A*A1(J)
PPTOT=T1*MB1
GPTOT=PPTOT
GO TO 90
88 IF(DTA1B1.GE.0.00)GO TO 90

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      WLC1=WLCN(PC1(2),PC1(1))
      CALL RIIP(R0,WLC1,WLC1,PLASD)
127  RM=HBE+HAE+R0
      H=HAE
      NOELAY=.FALSE.
      IF(FCE.GT.0.00)GO TO 129
      FCE=1.0-2
      NOELAY=.TRUE.
129  F=FREQ/FCE
130  IF(.NOT.FLAG)GO TO 1305
      CBET1= DABS(Z10PP)/RM
      SBET1=DSQRT(1.00-CBET1**2)
      Y3P=RM*SBET1
      YBEP=(R0+HBE)*SBET1
      GO TO 131
1305 Y3P=DSQRT(RM**2-P1P(3)**2)
      YBEP=DSQRT((R0+HBE)**2-P1P(3)**2)
C    EQN(18)
      CBET1=BCBC1/RM
      SBET1=DSQRT(1.00-CBET1*CBET1)
131  IF(F*SBET1.GT.1.00) GO TO 135
      IF(FLAG) GO TO 134
132  IF(FLAG2) GO TO 134
1325 IREFL=1
      RM=R0+HBE+HAE
      MR3=A1MAG
      SIN02=DOT(A1,B1)/(MB1*A1MAG)
      COS02=DSQRT(1.00-SIN02**2)
      Y9P=P1P(2)
      Z9P=P1P(3)
      C22P=L(2,1)*B1(1)+L(2,2)*B1(2)+L(2,3)*B1(3)
      C23P=L(3,1)*B1(1)+L(3,2)*B1(2)+L(3,3)*B1(3)
      Y10P=COS02*(Y9P*COS02+Z9P*SIN02)
      Z10P=COS02*(Z9P*COS02-Y9P*SIN02)
      GO TO 3096
134  FLAG=.FALSE.
      ISTOP=11
      GO TO 7310
135  IF(.NOT.NOELAY) GO TO 137
      Y4P=Y3P
      DGP1=0.00
      Z4P=P1P(3)
      GO TO 139
137  DGP1=-H/SBET1+H*F/2.00*DL0G((F*SBET1+1.00)/(F*SBET1-1.00))
      GAM1=CBET1*DGP1/RM
      Y4P=Y3P*DCOS(GAM1)-P1P(3)*DSIN(GAM1)
      Z4P=P1P(3)*DCOS(GAM1)+Y3P*DSIN(GAM1)
C    DIST BETWEEN SUCCESSIVE R<S
139  DISTB=DSQRT((Y4P-Y5P)**2+(Z4P-Z5P)**2)
      IF(FLAG) GO TO 141
      DO 140 J=1,3
140  P4(J)=L(2,J)*Y4P+L(3,J)*Z4P
      GO TO 1418
141  DO 1413 J=1,3
1413 P4(J)=M(2,J)*Y4P+M(3,J)*Z4P+P0(J)
1418 IF(DISTB.LE.EPS1) GO TO 200
      IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 145

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	OUT2=DISTA	TR2
	IF(IWRITE.EQ.1) WRITE(6,142) OUT2, IHOPS	TR2
142	FORMAT(24H E-LAYER CONV. PROBLEMS,,F6.1,17H KM USED, HOP NO.,I3)	TR2
	H=HP	TR2
	Y3P=Y3PP	TR2
	RM=RMP	TR2
	DGP1=GPP	TR2
	F=FP	TR2
	GO TO 215	TR2
145	NL4=DASIN(P4(3)/MAG(P4))	TR2
	WL4=WLON(P4(2),P4(1))	TR2
	DISTA=DISTB	TR2
	GPP=DGP1	TR2
	Y5P=Y4P	TR2
	Z5P=Z4P	TR2
	HP=H	TR2
	FP=F	TR2
	Y3PP=Y3P	TR2
	RMP=RM	TR2
	SIN01=SBET1	TR2
	COS01=CBET1	TR2
	DO 148 J=1,3	TR2
148	R2(J)=P4(J)	TR2
	CALL RIIP(R0,NL4,WL4,PLASD)	TR2
	NOELAY=.FALSE.	TR2
	IF(FCE.GT.0.00) GO TO 149	TR2
	FCE=1.0-2	TR2
	NOELAY=.TRUE.	TR2
149	RM=HBE+HAE*R0	TR2
	H=HAE	TR2
	F=FREQ/FCE	TR2
	INT=INT+1	TR2
	IF(INT.LE.LIMEA) GO TO 130	TR2
	ISTOP=12	TR2
	GO TO 7310	TR2
C	END OF E LAYER REFRACTION	TR2
C	START OF F1 LAYER REFRACTION	TR2
200	Y5P=Y4P	TR2
	Z5P=Z4P	TR2
	SIN01=SBET1	TR2
	COS01=CBET1	TR2
	DO 210 J=1,3	TR2
210	R2(J)=P4(J)	TR2
215	MR2=RM	TR2
	RR1=MR2-H	TR2
	SIN01P=SIN01	TR2
	COS01P=COS01	TR2
	Y6P=COS01*(Y5P*COS01+Z5P*SIN01)	TR2
	Z6P=COS01*(Z5P*COS01-Y5P*SIN01)	TR2
	IF(.NOT.FLAG) GO TO 2155	TR2
	DO 2151 J=1,3	TR2
2151	P4(J)=H(2,J)*Y3P+H(3,J)*Z10PP	TR2
	RR1=-H/MAG(P4)	TR2
	DO 2152 J=1,3	TR2
2152	P4(J)=R2(J)+RR1*P4(J)	TR2
	RR1=MAG(P4)	TR2
	MR2=MAG(R2)	TR2

	COS01P=BCBC1/MR2	TR2
	SIN01P=DSQRT(1.00-COS01P**2)	TR2
	DO 2153 J=1,3	TR2
	P4(J)=M(2,J)*Y6P+M(3,J)*Z6P+P0(J)	TR2
2153	P8(J)=R2(J)-P4(J)	TR2
	CALL CROSS(R2,P8,XI)	TR2
	CALL CROSS(XI,P8,KP)	TR2
	CNST=MAG(XI)	TR2
	FLOG=MAG(P8)	TR2
	DO 2154 J=1,3	TR2
	L(1,J)=XI(J)/CNST	TR2
	L(2,J)=P8(J)/FLOG	TR2
2154	L(3,J)=KP(J)/(CNST*FLOG)	TR2
	Y5P=L(2,1)*R2(1)+L(2,2)*R2(2)+L(2,3)*R2(3)	TR2
	Z5P=L(3,1)*R2(1)+L(3,2)*R2(2)+L(3,3)*R2(3)	TR2
	Y6P=L(2,1)*P4(1)+L(2,2)*P4(2)+L(2,3)*P4(3)	TR2
	Z6P=L(3,1)*P4(1)+L(3,2)*P4(2)+L(3,3)*P4(3)	TR2
	FLAG=.FALSE.	TR2
2155	INT=0	TR2
	FLAG3=.FALSE.	TR2
	HEA=H	TR2
	HE=H	TR2
	PPEF1A=0.00	TR2
	IF(.NOT.NOELAY)PPEF1A=H*(.500*SIN01-1.00/SIN01+F/4.00*(1.00-F**(-2	TR2
	)+COS01**2)*DLOG((F*SIN01+1.00)/(F*SIN01-1.00))	TR2
	JPP1=PPEF1A	TR2
	P0=RR1*DSQRT(1.00-(COS01P*MR2/RR1)**2)	TR2
	1AU1EA=MR2*SIN01P-P0	TR2
	IF(.NOT.HITS.OR.COS01P*MR2/A1MAG.GE.1.00) GO TO 217	TR2
	PP0=PP0-A1MAG*DSQRT(1.00-(COS01P*MR2/A1MAG)**2)	TR2
217	C12P=Y5P-Y6P	TR2
	C13P=Z5P-Z6P	TR2
	MC1PSQ=C12P**2+C13P**2	TR2
	MRX1SQ=BCBC1**2	TR2
218	RM=R0+HBE+HAE+HAF1	TR2
	TC2=DSQRT((RM**2-MRX1SQ)/MC1PSQ)	TR2
	IF(SEARCH.AND.RTARG.GT.DSQRT(MRX1SQ).AND.RTARG.LE.RR1) GO TO 591	TR2
	YC2P=C12P*TC2+Y6P	TR2
	ZC2P=C13P*TC2+Z6P	TR2
	DO 220 J=1,3	TR2
220	PC2(J)=L(2,J)*YC2P+L(3,J)*ZC2P	TR2
	NLC2= DASIN(PC2(3)/RM)	TR2
	WLC2=WCON(PC2(2),PC2(1))	TR2
	CALL PIIF(R0,NLC2,WLC2,PLASD)	TR2
225	RM=R0+HBE+HAE+HAF1	TR2
	H=HAF1	TR2
	F=FREQ/FCF1	TR2
	Y9P=0.00	TR2
	Z9P=0.00	TR2
230	IF(.NOT.FLAG) GO TO 2305	TR2
	CBET4= DABS(Z10PP)/RM	TR2
	SBET4=DSQRT(1.00-CBET4**2)	TR2
	Y7P=RM*SBET4	TR2
	GO TO 231	TR2
2305	TDEL3=DSQRT((RM**2-MRX1SQ)/MC1PSQ)	TR2
	Y7P=C12P*TDEL3+Y6P	TR2
	Z7P=C13P*TDEL3+Z6P	TR2

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      MR3=RM
      CBET4=BCBC1/MR3
      SBET4=DSQRT(1.00-CBET4*CBET4)
231  IF(F*SBET4.GT.1.00) GO TO 235
      IF(FLAG) GO TO 234
232  IF(FLAG3) GO TO 234
2325 IREFL=2
      RM=R0+HRE+HAE+HAF1
      Y9P=Y5P
      Z9P=Z5P
      MR3=MR2
      COS02=COS01
      SIN02=SIN01
      Y10P=COS02*(Y9P*COS02+Z9P*SIN02)
      Z10P=COS02*(Z9P*COS02-Y9P*SIN02)
      GO TO 3095
234  FLAG=.FALSE.
      ISTOP=13
      GO TO 7310
235  DGP2=H*(F/2.00*DLOG((F*SBET4+1.00)/(F*SBET4-1.00))-1.00/SBET4)
      GAM2=CBET4*DGP2/RM
      Y8P=Y7P*DCOS(GAM2)-Z7P*DSIN(GAM2)
      Z8P=Z7P*DCOS(GAM2)+Y7P*DSIN(GAM2)
C    DIST BETWEEN SUCCESSIVE R<S
      DISTB=DSQRT((Y8P-Y9P)**2+(Z8P-Z9P)**2)
      IF(FLAG) GO TO 241
      DO 240 J=1,3
240  P8(J)=L(2,J)*Y8P+L(3,J)*Z8P
      GO TO 2425
241  DO 242 J=1,3
242  P8(J)=M(2,J)*Y8P+M(3,J)*Z8P+P0(J)
2425 IF(DISTB.LE.EPS2) GO TO 300
      IF(INT.LE.1.OR.DISTB.LT.DISTA)GO TO 245
      OUT2=OISTA
      IF(IWRITE.EQ.1)WRITE(6,243)OUT2,IHOPS
243  FORMAT(25H F1-LAYER CONV. PROBLEMS,,F6.1,17H KM USED, HOP NO.,I3)
      H=HP
      F=FP
      Y7P=Y7PP
      RM=RMP
      DGP2=GPP
      GO TO 307
245  NL8= DASIN(P8(3)/MAG(P8))
      WL8=WLON(P8(2),P8(1))
      Y9P=Y8P
      Z9P=Z8P
      HP=H
      FP=F
      Y7PP=Y7P
      RMP=RM
      GPP=DGP2
      COS02=CBET4
      SIN02=SBET4
      DO 247 J=1,3
247  R3(J)=P8(J)
      OISTA=DISTB
      CALL RIIP(R0,NL8,WL8,PLASD)

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      HF1=H
      TAU=MR3*SINO2P-RR2*DSQRT(1.00-(MR3/RR2*COS02P)**2)+TAU1EA
      PPEF1A=PPEF1A+H*(.500*SINO2+F/4.00*(1.00-F**(-2)+COS02**2)*DLOG((F
      **SINO2+1.00)/(F*SINO2-1.00))-1.00/SINO2)+TAU
      GPEF1A=OGP1+OGP2+TAU
3095  C22P=Y9P-Y10P
      C23P=Z9P-Z10P
3096  TC3=(RM**2-Y10P**2-Z10P**2)/(C22P**2+C23P**2)
      IF(TC3.LT.0.00)GO TO (134,134,234),IREFL
      TC3=DSQRT(TC3)
      YC3P=C22P*TC3+Y10P
      ZC3P=C23P*TC3+Z10P
      DO 310 J=1,3
      PC3(J)=L(2,J)*YC3P+L(3,J)*ZC3P
      P10(J)=L(2,J)*Y10P+L(3,J)*Z10P
310   C2(J)=L(2,J)*C22P+L(3,J)*C23P
      BETA22=0.00
      NLC3=DASIN(PC3(3)/RM)
      WLC3=WCON(PC3(2),PC3(1))
      NOFLAG=0
      CALL HTGROF(NOFLAG,FREQ,RTD*NLC3,RTD*WLC3,RTD*DACOS(BCBC1/RM),0.
      *00,RM,RM1,RT1,RTM1,DNDR,DNDNL,DNDWL,PNTFLG)
      NOFLAG=1
      GO TO (311,312,313),IREFL
311   F1=FREQ/FCE
      H1=HAE
      IF(NUSE.EQ.1) GO TO 314
      FLAG2=.TRUE.
      INT=0
      GO TO 127
312   F1=FREQ/FCF1*.86602540378443900
      RM1=RM1+HAF1
      H1=HAF1*2.00
      GO TO (3123,314,3125),NUSE
3123  IF(FLAG2) GO TO 134
      FLAG2=.TRUE.
      GO TO 1325
3125  FLAG3=.TRUE.
      INT=0
      GO TO 225
313   F1=FREQ/FCF2
      H1=HAF2
      IF(NUSE.EQ.3) GO TO 314
      IF(FLAG3) GO TO 234
      FLAG3=.TRUE.
      GO TO 2325
314   INTF2=0
      IRCYCL=0
315   COPHC3=PC3(3)/RM
      SIPHC3=DSQRT(1.00-COPHC3**2)
      NNUSE(INUSE)=NUSE
      FCREP(INUSE)=FREQ/F1
C     CORRECTION IN F1 CRITICAL PRINT OUT
      IF(NUSE.EQ.2) FCREP(INUSE)=FCF1
      COTH3=PC3(1)/DSQRT(PC3(1)**2+PC3(2)**2)
      SITH3=PC3(2)/DSQRT(PC3(1)**2+PC3(2)**2)
      PR1(1)=RTM1*COTH3*SIPHC3

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PR1(2)=RTM1*SITHC3*SIPHC3 TR2
PR1(3)=RTM1*COPHC3 TR2
N1(1)=COTH3*SIPHC3*DNDR-COTH3*COPHC3*DNDNL/RTM1+SITHC3*DNDWL/(RT TR2
*M1*SIPHC3) TR2
N1(2)=SITH3*SIPHC3*DNDR-SITH3*COPHC3*DNDNL/RTM1-COTH3*DNDWL/(RT TR2
*M1*SIPHC3) TR2
N1(3)=COPHC3*DNDR+SIPHC3*DNDNL/RTM1 TR2
MN1=MAG(N1) TR2
T0=-RTM1/MN1 TR2
ISTOP=1 TR2
DO 320 J=1,3 TR2
P0(J)=N1(J)*T0+PR1(J) TR2
320 A2(J)=P10(J)-P0(J) TR2
CALL CROSS(A2,C2,XI) TR2
CALL CROSS(XI,C2,KP) TR2
MA2C2=MAG(XI) TR2
MC2=MAG(C2) TR2
DO 330 J=1,3 TR2
M(1,J)=XI(J)/MA2C2 TR2
M(2,J)=C2(J)/MC2 TR2
330 M(3,J)=KP(J)/(MA2C2*MC2) TR2
Z10PP=M(3,1)*A2(1)+M(3,2)*A2(2)+M(3,3)*A2(3) TR2
RB=RM1-M1 TR2
IF(PB.GE.DABS(Z10PP))GO TO 332 TR2
ISTOP=2 TR2
GO TO 3345 TR2
332 COBETB= DABS(Z10PP)/RB TR2
SIBETB=DSQRT(1.00-COBETB**2) TR2
YS1PP=RB*SIBETB TR2
DO 333 J=1,3 TR2
333 S1(J)=M(2,J)*YS1PP+M(3,J)*Z10PP+P0(J) TR2
R4=MAG(S1) TR2
PP2=1.00-(MR3/R4*COS02)**2 TR2
IF(PP2.GE.0.00) GO TO 3331 TR2
ISTOP=2 TR2
GO TO 3345 TR2
3331 PP2=R4*DSQRT(PP2)-MR3*SIN02 TR2
PP2A=PP2 TR2
IF(IREFL.GT.1) GO TO 3336 TR2
IF(HITS) GO TO 3334 TR2
PP0=R4*DSQRT(1.00-(MR3/R4*COS02)**2) TR2
GO TO 3336 TR2
3334 PP0=PP2 TR2
3336 CBTTM1=RB*COBETB/RTM1 TR2
IF(CBTTM1.LE.1.00)GO TO 334 TR2
ISTOP=3 TR2
GO TO 3345 TR2
334 SBTTM1=DSQRT(1.00-CBTTM1**2) TR2
FLAG=.FALSE. TR2
IF(1.00-F1*SBTTM1.GT.0.00) GO TO 335 TR2
FLAG=.TRUE. TR2
3345 THETA=1.00/RTM1 TR2
DIST1=1.010 TR2
IRCYCL=0 TR2
GO TO 336 TR2
335 FLOG=M1*F1*DLOG((1.00+F1*SBTTM1)/(1.00-F1*SBTTM1))/2.00 TR2
GPF2=FLOG*2.00 TR2

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      F=FP
      RM=RMP
      YOPPP2=YOPPP
      OUT2=DISTA
      IF(IWRITE.EQ.1)WRITE(6,243)OUT2,IHOPS
      GO TO 390
384  YOPPP=YOPPP2
      DISTA=DISTB
      RMP=RM
      FP=F
      HP=H
      INT=INT+1
      IF(INT.LE.LIMF1D) GO TO 370
      ISTOP=4
      IRCYCL=0
      GO TO 475
C   E LAYER DOWNWARD
390  YM1PPP=YOPPP2
      HF1=H
      MRM1=DSQRT(YM1PPP**2+ZS3PPP**2)
      DO 395 J=1,3
395  RN1(J)=P(2,J)*YM1PPP+P(3,J)*ZS3PPP
      SBETM1=DABS(DOT(RN1,C3)/(MRM1*MC3))
      CBETM1=DSQRT(1.00-SBETM1*SBETM1)
      R4=MAG(A3)
      PP2=PP2+R4*DSQRT(1.00-(MRM1/R4*CBETM1)**2)-MRM1*SBETM1
      IF(F*SBETM1.GT.1.00)GO TO 398
      ISTOP=5
      IRCYCL=0
      GO TO 475
398  FLOG=DL0G((F*SBETM1+1.00)/(F*SBETM1-1.00))
      DGP2P=H*(F/2.00*FLOG-1.00/SBETM1)
      TH12=CBETM1*DGP2P/RM
      PPEF10=H*(.500*SBETM1+F/4.00*(1.00-F**(-2)+CBETM1**2)*FLOG-1.00/SB
*ETM1)
      DPP2P=PPEF10
      RR2=MRM1*SBETM1
      RR2C=MRM1*CBETM1
      YM2PPP=YM1PPP*DCOS(TH12)-ZS3PPP*DSIN(TH12)
      ZM2PPP=ZS3PPP*DCOS(TH12)+YM1PPP*DSIN(TH12)
      MRM2=DSQRT(YM2PPP**2+ZM2PPP**2)
      YY1PPP=CBETM1*(YM2PPP*CBETM1-ZM2PPP*SBETM1)
      ZY1PPP=CBETM1*(ZM2PPP*CBETM1+YM2PPP*SBETM1)
      C42PPP=YY1PPP-YM2PPP
      C43PPP=ZY1PPP-ZM2PPP
      MRY1SQ=YY1PPP**2+ZY1PPP**2
      MC4SQ=C42PPP**2+C43PPP**2
3984 IF(MR2**2.GE.MRY1SQ)GO TO 399
      IF(B**2.GE.MRY1SQ) GO TO 3986
      ISTOP=6
      IRCYCL=0
      GO TO 475
3986 TE=DSQRT((B**2-MRY1SQ)/MC4SQ)
      RM=B
      GO TO 3995
3987 CNST=-DOT(A3,C3)/MC3**2
      C42PPP=P(2,1)*C3(1)+P(2,2)*C3(2)+P(2,3)*C3(3)

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      C43PPP=P(3,1)*C3(1)+P(3,2)*C3(2)+P(3,3)*C3(3)      TR2
      YY1PPP=YS3PPP+CNST*C42PPP      TR2
      ZY1PPP=ZS3PPP+CNST*C43PPP      TR2
      MRY1SQ=YY1PPP**2+ZY1PPP**2      TR2
      MC4SQ=MC3**2      TR2
      MRM1=DSQRT(YS3PPP**2+ZS3PPP**2)      TR2
      CBETH1=DSQRT(MRY1SQ)/MRM1      TR2
      SBETH1=DSQRT(1.00-CBETH1**2)      TR2
      GO TO 3984      TR2
399    TE=-DSQRT((MR2**2-MRY1SQ)/MC4SQ)      TR2
3995   YEPPP=C42PPP*TE+YY1PPP      TR2
      ZEPPP=C43PPP*TE+ZY1PPP      TR2
C    E  LAYER ITERATION 400 TO 420      TR2
      INT=0      TR2
400    DO 410 J=1,3      TR2
410    PE(J)=P(2,J)*YEPPP+P(3,J)*ZEPPP      TR2
      NLE=DASIN(PE(3)/MAG(PE))      TR2
      WLE=WLON(PE(2),PE(1))      TR2
      CALL RIIP(R0,NLE,WLE,PLASD)      TR2
      NOELAY=.FALSE.      TR2
      IF(FCE.GT.0.00) GO TO 4105      TR2
      FCE=1.0-2      TR2
      NOELAY=.TRUE.      TR2
4105   RM=HBE+HAE+R0      TR2
      H=HAE      TR2
      F=FREQ/FCE      TR2
      IF(RM**2.GE.MRY1SQ) GO TO 411      TR2
      ISTOP=6      TR2
      IRCYCL=0      TR2
      GO TO 475      TR2
411    TE=-DSQRT((RM**2-MRY1SQ)/MC4SQ)      TR2
      YEPPP2=C42PPP*TE+YY1PPP      TR2
      ZEPPP2=C43PPP*TE+ZY1PPP      TR2
      DISTB=DSQRT((YEPPP-YEPPP2)**2+(ZEPPP-ZEPPP2)**2)      TR2
      IF(DISTB.LE.EPS4) GO TO 420      TR2
      IF(INT.LE.1.OR.DISTB.LT.DISTA) GO TO 414      TR2
      H=HP      TR2
      F=FP      TR2
      RM=RMP      TR2
      YEPPP2=YEPPP      TR2
      ZEPPP2=ZEPPP      TR2
      OUT2=DISTA      TR2
      IF(IWRITE.EQ.1)WRITE(6,142)OUT2,IHOPS      TR2
      GO TO 420      TR2
414    YEPPP=YEPPP2      TR2
      ZEPPP=ZEPPP2      TR2
      RMP=RM      TR2
      FP=F      TR2
      HP=H      TR2
      DISTA=DISTB      TR2
      INT=INT+1      TR2
      IF(INT.LE.LIMED) GO TO 400      TR2
      ISTOP=7      TR2
      IRCYCL=0      TR2
      GO TO 475      TR2
420    YM3PPP=YEPPP2      TR2
      ZM3PPP=ZEPPP2      TR2

```

	HE=H	TR2
C	END OF E LAYER	TR2
	MRM3=DSQRT(YM3PPP**2+ZM3PPP**2)	TR2
	CBETH2=MRM1*CBETH1/MRM3	TR2
	SBETH2=DSQRT(1.00-CBETH2*CBETH2)	TR2
	IF(IREFL.EQ.2) PP2=PP2+MRM1*SBETH1-MRM3*SBETH2	TR2
	IF(F*SBETH2.GT.1.00) GO TO 430	TR2
	ISTOP=8	TR2
	IRCYCL=0	TR2
	GO TO 475	TR2
430	IF(.NOT.NOELAY) GO TO 4302	TR2
	FLOG=0.00	TR2
	DPP1P=0.00	TR2
	TH34=0.00	TR2
	DGP1P=0.00	TR2
	YM4PPP=YM3PPP	TR2
	ZM4PPP=ZM3PPP	TR2
	MRM4=MRM3	TR2
	GO TO 4304	TR2
4302	FLOG=DL0G((F*SBETH2+1.00)/(F*SBETH2-1.00))	TR2
	DGP1P=H*(F/2.00*FLOG-1.00/SBETH2)	TR2
	TH34=CBETH2*DGP1P/RH	TR2
	YM4PPP=YM3PPP*DCOS(TH34)-ZM3PPP*DSIN(TH34)	TR2
	ZM4PPP=ZM3PPP*DCOS(TH34)+YM3PPP*DSIN(TH34)	TR2
	MRM4=DSQRT(YM4PPP**2+ZM4PPP**2)	TR2
	DPP1P=H*(.500*SBETH2+F/4.00*(1.00-F**(-2)+CBETH2**2)*FLOG-1.00/SBETH2)	TR2
4304	RR1=MRM4-H	TR2
	IF(IREFL.LT.3) GO TO 4305	TR2
	IF(DABS(RR2C).GT.RR1) GO TO 431	TR2
	TAU=RR2-RR1*DSQRT(1.00-(RR2C/RR1)**2)	TR2
	PPEF10=PPEF1D+DPP1P+TAU	TR2
	GPEF10=DGP1P+DGP2P+TAU	TR2
4305	YY2PPP=CBETH2*(YM4PPP*CBETH2-ZM4PPP*SBETH2)	TR2
	ZY2PPP=CBETH2*(ZM4PPP*CBETH2+YM4PPP*SBETH2)	TR2
	C52PPP=YY2PPP-YM4PPP	TR2
	C53PPP=ZY2PPP-ZM4PPP	TR2
	MC5SQ=C52PPP**2+C53PPP**2	TR2
	SBM4H2=1.00-(CBETH2/(1.00-HE/MRM4))**2	TR2
	IF(SBM4H2.GT.0.00) GO TO 4307	TR2
	ISTOP=15	TR2
	IRCYCL=0	TR2
	GO TO 475	TR2
4307	TAU1ED=MRM4*SBETH2-(MRM4-HE)*DSQRT(SBM4H2)	TR2
	RY=DSQRT(MRY1SQ)	TR2
	GO TO 437	TR2
431	ISTOP=9	TR2
	IRCYCL=0	TR2
	GO TO 475	TR2
436	MB1=MAG(A3)	TR2
	SBET1=-DOT(A3,C3)/(MB1*MC3)	TR2
	CBET1=DSQRT(1.00-SBET1**2)	TR2
	RY=MB1*CBET1	TR2
	MRY1SQ=RY**2	TR2
	CNST=MB1/MC3*SBET1	TR2
	C52PPP=P(2,1)*C3(1)+P(2,2)*C3(2)+P(2,3)*C3(3)	TR2
	C53PPP=P(3,1)*C3(1)+P(3,2)*C3(2)+P(3,3)*C3(3)	TR2

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YY2PPP=YS3PPP+CNST*C52PPP
ZY2PPP=ZS3PPP+CNST*C53PPP
MC5SQ=MC3**2
437 HITS=R0.GT.RY
INCHOP=(R0+50.00).GE.RY
IF(R0+HBE.GT.RY) GO TO 438
ISTOP=15
IRCYCL=0
GO TO 475
438 TQ=-DSQRT(((R0+HBE)**2-MRY1SQ)/MC5SQ)
YBEP= C52PPP*TQ+YY2PPP
ZBEP= C53PPP*TQ+ZY2PPP
IF(.NOT.HITS) GO TO 450
TQ=-DSQRT((R0**2-MRY1SQ)/MC5SQ)
YQPPP=C52PPP*TQ+YY2PPP
ZQPPP=C53PPP*TQ+ZY2PPP
DO 440 J=1,3
440 PQ(J)=P(2,J)*YQPPP+P(3,J)*ZQPPP
GO TO 461
450 DO 460 J=1,3
460 PQ(J)=P(2,J)*YY2PPP+P(3,J)*ZY2PPP
C STARTS TO ITERATE TILTED F2
461 DIST2=DSQRT((PQ(1)-PREV(1))**2+(PQ(2)-PREV(2))**2+(PQ(3)-PREV
*(3))**2)
RTDIF=DABS(RT1-PREV(13))
IF(IRCYCL.LE.2) GO TO 475
IF(DIST2-EPS5) 463,463,462
462 IF(DIST1-DIST2) 470,475,475
463 IF(RTDIF-EPS5) 500,500,475
470 CALL PRVGET
ICNPRB=1
IF(IWRITE.EQ.1) WRITE(6,473) IHOPS,EPS5,DIST1,RTDIF
473 FORMAT(48H TILTED LAYER CONVERGENCE PROBLEMS ON HOP NUMBER,I3,
1 1H,,F6.1,29H KM. CRITERIA NOT MET, DIST1=,F8.2,8H, RTDIF=,
2 F8.2)
GO TO 500
475 YW2PP=RTM1*YS2PP/RB
ZW2PP=RTM1*ZS2PP/RB
DO 480 J=1,3
480 PW2(J)=M(2,J)*YW2PP+M(3,J)*ZW2PP+P0(J)
NLW2=DASIN(PW2(3)/MAG(PW2))
HLW2=HLON(PW2(2),PW2(1))
DO 490 J=1,3
490 W2(J)=PW2(J)-P0(J)
BETA22=DACOS(DOT(PW2,W2)/(MAG(W2)*MAG(PW2)))
BETTM1=DASIN(SBTMM1)
CALL PRVSTO
DIST1=DIST2
BP=RTM1
CALL HTSRDF(NDFLAG,FREQ,RTD*NLW2,RTD*HLW2,RTD*BETTM1,RTD*BETA22,8
*P,RM1,RT1,RTM1,DNDR,DNDL,DNDL,DNDL,DNDL)
IF(IREFL.NE.NUSE) GO TO 501
GO TO (4916,4917,4918),IREFL
4916 F1=FREQ/FCE
H1=HAE
GO TO 4919
4917 F1=FREQ/FCF1*.86602540378443900

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ROUTINE TRISL

74/74 OPT=1

FTN 4.5+414

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	RM1=RM1+HAF1	TR2
	H1=HAF1*2.00	TR2
	GO TO 4919	TR2
4918	F1=FREQ/FCF2	TR2
	H1=HAF2	TR2
4919	INTF2=INTF2+1	TR2
	RM=MAG(PW2)	TR2
	DO 492 J=1,3	TR2
492	PG3(J)=PW2(J)	TR2
	IF (INTF2.LE.LIMF2) GO TO 315	TR2
	IF (ISTOP.GT.1) GO TO 7310	TR2
494	IF (FLAG.OR.PNTFLG.GT.500) GO TO 501	TR2
	GO TO 7310	TR2
C	ITERATION FINISHED	TR2
500	DO 5003 J=1,3	TR2
	VEC(J,1)=L(2,J)	TR2
	LOC(J,1)=L(2,J)*YBEP+L(3,J)*P1P(3)	TR2
	VEC(J,2)=L(2,J)*C12P+L(3,J)*C13P	TR2
	LOC(J,2)=R2(J)	TR2
	VEC(J,3)=M(2,J)	TR2
	LOC(J,3)=L(2,J)*Y9P+L(3,J)*Z9P	TR2
	VEC(J,4)=P(2,J)	TR2
	LOC(J,4)=M(2,J)*YS1PP+M(3,J)*Z10PP+P0(J)	TR2
	LOC(J,5)=A3(J)	TR2
	LOC(J,6)=P(2,J)*YM1PPP+P(3,J)*ZS3PPP	TR2
	VEC(J,5)=P(2,J)*C42PPP+P(3,J)*C43PPP	TR2
	LOC(J,7)=P(2,J)*YM3PPP+P(3,J)*ZM3PPP	TR2
	VEC(J,6)=P(2,J)*C52PPP+P(3,J)*C53PPP	TR2
5003	LOC(J,8)=P(2,J)*YBEP+P(3,J)*ZBEP	TR2
	DO 5008 K=1,6	TR2
	MAGVEC=MAG(VEC(1,K))	TR2
	IF (MAGVEC.EQ.0.00) GO TO 5008	TR2
	DO 5007 J=1,3	TR2
5007	VEC(J,K)=VEC(J,K)/MAGVEC	TR2
5008	CONTINUE	TR2
	IF (PNTFLG.LT..5) GO TO 510	TR2
501	IF (FLAG2) GO TO 134	TR2
	IF (FLAG3) GO TO 234	TR2
	RM=RM1	TR2
	INT=0	TR2
	FLAG=.TRUE.	TR2
	GO TO (502,503,504), IREFL	TR2
502	CBET1=COBETB*RB/RM	TR2
	FLAG2=.TRUE.	TR2
	SBET1=DSQRT(1.00-CBET1**2)	TR2
	Y3P=DSQRT(RM**2-Z10PP**2)	TR2
	P1P(3)=Z10PP	TR2
	F=FREQ/FCF	TR2
	H=HAE	TR2
	GO TO 131	TR2
503	F=FREQ/FCF1	TR2
	FLAG3=.TRUE.	TR2
	H=HAF1	TR2
	MR3=RM	TR2
	CBET4=COBETB*RB/RM	TR2
	IF (DABS(CBET4).LT.1.00.AND.DABS(RM).GT.DABS(Z10PP)) GO TO 5035	TR2
	ISTOP=6	TR2

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      IRCYCL=0
      GO TO 475
5035 SBET4=DSQRT(1.00-CBET4**2)
      Y7P=DSQRT(RM**2-Z10PP**2)
      Z7P=Z10PP
      GO TO 231
504  IF(IWRITE.EQ.1)WRITE(6,505)IHOPS
505  FORMAT(23H PENETRATION ON HOP NO.,I3,1H.)
      GO TO 7311
510  IF(HITS) GO TO 530
      GO TO (512,514,514),IREFL
512  PP0P=MB1*SBET1
      GO TO 516
514  PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)
516  DO 520 J=1,3
      B1(J)=P(2,J)*C52PPP+P(3,J)*C53PPP
520  A1(J)=PQ(J)
      GO TO 550
530  GO TO (531,532,532),IREFL
531  ALPHAQ=DASIN(MB1/R0*CBET1)
      PP0P=MB1*SBET1-R0*DSQRT(1.00-(RY/R0)**2)
      GO TO 533
532  ALPHAQ=DASIN(MRM1*CBETM1/R0)
      PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)-R0*DSQRT(1.00-
      *0-(MRM4/R0*CBETM2)**2)
533  B22PPP=-C52PPP*DCOS(2.00*ALPHAQ)+C53PPP*DSIN(2.00*ALPHAQ)
      B23PPP=-C53PPP*DCOS(2.00*ALPHAQ)-C52PPP*DSIN(2.00*ALPHAQ)
      DO 540 J=1,3
      A1(J)=PQ(J)
540  B1(J)=P(2,J)*B22PPP+P(3,J)*B23PPP
550  IF(IHOPS.GE.IABS(MODE))GO TO 552
551  GO TO (5511,5512,5513),IREFL
5511 PPTOT=PPTOT+PP0+PPF2+PP0P
      GPTOT=GPTOT+PP0+GPF2+PP0P
      GO TO 5514
5512 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED
      GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED
      GO TO 5514
5513 PPTOT=PPTOT+PP0+PPEF1A+PPF2+PP2+PPEF1D+PP0P
      GPTOT=GPTOT+PP0+GPEF1A+GPF2+PP2+GPEF1D+PP0P
5514 MB1=MAG(A1)
      IF(.NOT.HITS.AND.IHOPS.GE.IABS(MODE).AND.MB1.GE.RTARG) GO TO 598
      GO TO 90
552  IF(SEARCH.AND.RTARG.GT.MR3-HF1A.AND.RTARG.LE.DMAX1(RV,MR3))GOTO595
      IF(ASC) GO TO 566
      IF(DABS(RTARG-R0).LE.1.0-5.AND.HITS) GO TO 580
      IF(MODE.GT.0) GO TO 563
C  DESCENDING MODE
      GO TO(564,562,560),IREFL
560  IF(RTARG.LE.DMAX1(RV,MRM1).AND.RTARG.GT.MRM1-HF1) GO TO 576
      IF(DMIN1(MRM4-4E,MRM1).LT.RTARG.AND.RTARG.LE.DMAX1(MRM4,MRM1-HF1))
      * GO TO 573
      IF(RTARG.LE.MRM4-HE) GO TO 568
      IF(INCHOP) GO TO 566
      SEARCH=.TRUE.
      GO TO 5513
562  IF(RTARG.LE.RV.AND.RTARG.GT.MRM4) GO TO 576

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      IF(RTARG.LE.MRM4) GO TO 568
      IF(INCHOP) GO TO 566
      SEARCH=.TRUE.
      GO TO 5512
563  SEARCH=.TRUE.
      ASC=.TRUE.
      GO TO 551
564  IF(RTARG.LE.RV) GO TO 568
      SEARCH=.TRUE.
      IF(.NOT.INCHOP) GO TO 5511
566  ISTOP=15
      GO TO 7310
      568 IF(RTARG.GE.RY.OR.INCHOP) GO TO 569
      SEARCH=.TRUE.
      GO TO 551
569  TTARG=0.00
      IF(RTARG.GT.RY) TTARG=-DSQRT((RTARG**2-MRY1SQ)/MC5SQ)
      YTARGP=C52PPP*TTARG+YY2PPP
      ZTARGP=C53PPP*TTARG+ZY2PPP
      DO 570 J=1,3
      B1(J)=C52PPP*P(2,J)+C53PPP*P(3,J)
570  PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP
      PP0P=0.00
      IF(RTARG.GT.RY) PP0P=-RTARG*DSQRT(1.00-(RY/RTARG)**2)
      GO TO (571,5715,5715),IREFL
571  PP0P=MB1*SBET1+PP0P
      PPTOT=PPTOT+PP0+PPF2+PP0P
      GPTOT=GPTOT+PP0+GPF2+PP0P
      GO TO 600
5715 PP0P=(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)+PP0P
      GO TO(5720,5720,5725),IREFL
5720 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED
      GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED
      GO TO 600
5725 PPTOT=PPTOT+PP0+PPEF1A+PPF2+PP2+PPEF1D+PP0P
      GPTOT=GPTOT+PP0+GPEF1A+GPF2+PP2+GPEF1D+PP0P
      GO TO 600
573  TTARG=-DSQRT((RTARG**2-MRY1SQ)/MC4SQ)
      YTARGP=C42PPP*TTARG+YY1PPP
      ZTARGP=C43PPP*TTARG+ZY1PPP
      DO 575 J=1,3
      B1(J)=C42PPP*P(2,J)+C43PPP*P(3,J)
575  PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP
      PPTOT=PPTOT+PPEF1A+PPF2+PP2+PP0+PPEF1D
      GPTOT=GPTOT+GPEF1A+GPF2+PP2+PP0+GPEF1D
      GO TO 600
576  YTARGP=-DSQRT(RTARG**2-ZS3PPP**2)
      ZTARGP=ZS3PPP
      DO 579 J=1,3
      B1(J)=C32PPP*P(2,J)
579  PTARG(J)=P(2,J)*YTARGP+P(3,J)*ZTARGP
      GO TO(5793,5793,5797),IREFL
5793 TAU=MRM4*SBETH2-(MRM4-HE)*DSQRT(1.00-(CBETM2/(1.00-HE/MRM4))**2)+P
      *P0+PP2
      PPTOT=PPTOT+TAU+DPP1+PPF2+TAU1EA
      GPTOT=GPTOT+TAU+DGP1+GPF2+TAU1EA
      GO TO 600

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5797 TAU=HRM1*SBETH1-(HRM1-HF1)*DSQRT(1.00-(CBETH1/(1.00-HF1/HRM4))**2) TF
      *+PP0+PP2 TR
      PPTOT=PPTOT+TAU+PPEF1A+PPF2+OPP2P TR
      GPTOT=GPTOT+TAU+GPEF1A+GPF2+DGP2P TR
      GO TO 600 TR
C TARGET ON GROUND TR
580 DO 590 J=1,3 TR
      B1(J)=C52PPP*P(2,J)+C53PPP*P(3,J) TR
590 PTARG(J)=A1(J) TR
      GO TO(5902,5904,5906),IREFL TR
5902 PPTOT=PPTOT+PP0+PPF2+PP0P TR
      GPTOT=GPTOT+PP0+GPF2+PP0P TR
      GO TO 600 TR
5904 PPTOT=PPTOT+PP0+DPP1+PPF2+PP2+DPP1P+PP0P+TAU1EA+TAU1ED TR
      GPTOT=GPTOT+PP0+DGP1+GPF2+PP2+DGP1P+PP0P+TAU1EA+TAU1ED TR
      GO TO 600 TR
5906 PPTOT=PPTOT+PP0+PPEF1A+PP2+PPF2+PPEF1D+PP0P TR
      GPTOT=GPTOT+PP0+GPEF1A+PP2+GPF2+GPEF1D+PP0P TR
      GO TO 600 TR
C ASCENDING MODE TR
591 YTARGP=DSQRT(RTARG**2-P1P(3)**2) TR
      DO 592 J=1,3 TR
592 PTARG(J)=L(2,J)*YTARGP+L(3,J)*P1P(3) TR
      TAU=RTARG*DSQRT(1.00-(RY/RTARG)**2) TR
      PPTOT=PPTOT+TAU TR
      GPTOT=GPTOT+TAU TR
      INUSE=INUSE-1 TR
      IF(.NOT.HITS) GO TO 600 TR
      TAU=-R0*DSQRT(1.00-(RY/R0)**2) TR
      PPTOT=PPTOT+TAU TR
      GPTOT=GPTOT+TAU TR
      GO TO 600 TR
593 TTARG=DSQRT((RTARG**2-HRX15Q)/HC1PSQ) TR
      YTARGP=C12P*TTARG+Y6P TR
      ZTARGP=C13P*TTARG+Z6P TR
      DO 594 J=1,3 TR
      PTARG(J)=L(2,J)*YTARGP+L(3,J)*ZTARGP TR
594 B1(J)=L(2,J)*C12P+L(3,J)*C13P TR
      TAU=(MR3-HF1A)*DSQRT(1.00-(COS02/(1.00-HF1A/MR3))**2) TR
      PPTOT=PPTOT+OPP1+TAU TR
      GPTOT=GPTOT+DGP1+TAU TR
      INUSE=INUSE-1 TR
      IF(.NOT.HITS) GO TO 600 TR
      TAU=-R0*DSQRT(1.00-((MR2-HEA)/R0*COS01)**2) TR
      PPTOT=PPTOT+TAU TR
      GPTOT=GPTOT+TAU TR
      GO TO 600 TR
595 TTARG=DSQRT((RTARG**2-Y10P**2-Z10P**2)/(C22P**2+C23P**2)) TR
      YTARGP=C22P*TTARG+Y10P TR
      ZTARGP=C23P*TTARG+Z10P TR
      DO 596 J=1,3 TR
      PTARG(J)=L(2,J)*YTARGP+L(3,J)*ZTARGP TR
596 B1(J)=L(2,J)*C12P+L(3,J)*C13P TR
      TAU=(MR2-HEA)*DSQRT(1.00-(COS01/(1.00-HEA/MR2))**2)+PP2A TR
      PPTOT=PPTOT+PPEF1A+PPF2/2.00+TAU TR
      GPTOT=GPTOT+GPEF1A+GPF2/2.00+TAU TR
      IF(.NOT.ASC) GO TO 600 TR

```

	INUSE=INUSE-1	TR2
	TAU=-R0*DSQRT(1.00-((MR2-HEA)/R0*COS01)**2)	TR2
	PPTOT=PPTOT+TAU	TR2
	GPTOT=GPTOT+TAU	TR2
	GO TO 600	TR2
598	RS2=MAG(A1)	TR2
	DO 599 I=1,3	TR2
599	PTARG(I)=A1(I)	TR2
	GO TO 601	TR2
600	IF(.NOT.HITS) RS2=MAG(PTARG)	TR2
601	IF(GPONLY) RETURN	TR2
	NLTARG=RTD*DASIN(PTARG(3)/RS2)	TR2
	WLTARG=RTD*WLOD(PTARG(2),PTARG(1))	TR2
	EAST(1)=-PTARG(2)	TR2
	EAST(2)=PTARG(1)	TR2
	EAST(3)=0.00	TR2
	CALL CROSS(PTARG,EAST,NORTH)	TR2
	CNST1=DOT(PTARG,B1)/RS2	TR2
	ELF=RTD*DASIN(CNST1/MAG(B1))	TR2
	ME=MAG(EAST)	TR2
	MN=MAG(NORTH)	TR2
	CNST=DOT(EAST,B1)/ME	TR2
	AZF=RTD*ATAN2(CNST,DOT(NORTH,B1)/MN)+180.00-DSIGN(180.00,CNST)	TR2
	B1(1)=PTARG(1)-A11(1)	TR2
	B1(2)=PTARG(2)-A11(2)	TR2
	B1(3)=PTARG(3)-A11(3)	TR2
	SRANGE=MAG(B1)	TR2
	ELSR=RTD*DASIN(DOT(A11,B1)/(SRANGE*MA1))	TR2
	DIST=R0*DACOS(DOT(A11,PTARG)/(RS2*MA1))	TR2
	CNST=DOT(EAST1,B1)	TR2
	BEAR=RTD*ATAN2(CNST,DOT(NORTH1,B1))+180.00-DSIGN(180.00,CNST)	TR2
	RETURN	TR2
7310	IGOBAK=1	TR2
	IF(IWRITE.EQ.1)WRITE(6,7309) MESSPR(ISTOP)	TR2
7309	FORMAT(11H MESSUP---,A10)	TR2
	RETURN	TR2
7311	IGOBAK=2	TR2
	RETURN	TR2
	END	TR2

FUNCTION MAG

74/74 OPT=1

FTN 4.5+414

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```
DOUBLE PRECISION FUNCTION MAG(A)
IMPLICIT DOUBLE PRECISION(A-Z)
DIMENSION A(3)
MAG=DSORT(A(1)*A(1)+A(2)*A(2)+A(3)*A(3))
RETURN
END
```

MAG  
MAG  
MAG  
MAG  
MAG  
MAG

FUNCTION DOT

74/74 OPT=1

FTN 4.5+414

04/27/

```
DOUBLE PRECISION FUNCTION DOT(A,B)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION A(3),B(3)
DOT=A(1)*B(1)+A(2)*B(2)+A(3)*B(3)
RETURN
END
```

DOT  
DOT  
DOT  
DOT  
DOT  
DOT

SUBROUTINE CROSS

74/74 OPT=1

FTN 4.5+414

04/27/

```
SUBROUTINE CROSS(A,B,C)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
DIMENSION A(3),B(3),C(3)
C(1)=A(2)*B(3)-A(3)*B(2)
C(2)=A(3)*B(1)-A(1)*B(3)
C(3)=A(1)*B(2)-A(2)*B(1)
RETURN
END
```

VEC  
VEC  
VEC  
VEC  
VEC  
VEC  
VEC  
VEC

ROUTINE PRVSTO 74/74 OPT=1

FTN 4.5+414

04/27/

	SUBROUTINE PRVSTO	PRV
	DOUBLE PRECISION P1,P2	PRV
	LOGICAL LP1,LP2	PRV
	COMMON/CPREV/P1(56),P2(56),LP1(6),LP2(6)	PRV
	DO 1 I=1,56	PRV
1	P2(I)=P1(I)	PRV
	DO 2 I=1,6	PRV
2	LP2(I)=LP1(I)	PRV
	RETURN	PRV
	ENTRY PRVGET	PRV
	DO 3 I=1,56	PRV
3	P1(I)=P2(I)	PRV
	DO 4 I=1,6	PRV
4	LP1(I)=LP2(I)	PRV
	RETURN	PRV
	END	PRV

ROUTINE HTGRDF 74/74 OPT=1

FTN 4.5+414

04/27/

	SUBROUTINE HTGRDF(NDFLAG,FREQ,NLAT,WLONG,ANGLE1,ANGLE2,RANG12,RMU	HTG
	*,RTU,RTMU,DNDR,DNDT,DNDP,PNTFLG)	HTG
	IMPLICIT DOUBLE PRECISION (A-H,O-Z)	HTG
	DOUBLE PRECISION NLAT,NLATR	HTG
	LOGICAL TILT,FAST	HTG
	COMMON/TILTG/TILT,FAST	HTG
	NLATR=NLAT/57.2957795130823200	HTG
	WLONGR=WLONG/57.2957795130823200	HTG
	CALL RIIP(6370.00,NLATR,WLONGR,EN)	HTG
	CALL RTFIND(NDFLAG,FREQ,ANGLE1,ANGLE2,RANG12,RTU,RMU,RTMU,PNTFLG)	HTG
	IF(TILT) GO TO 1	HTG
	DNDR=1.000	HTG
	DNDP=0.000	HTG
	DNDT=0.000	HTG
	RETURN	HTG
1	CALL DENSE(RTU,NLAT,WLONG,EN,DNDR,DNDT,DNDP)	HTG
	RETURN	HTG
	END	HTG

```

      SUBROUTINE RTFIND(NDFLAG,FREQ,ANGLE1,ANGLE2,RANG12,RTU,RMU,RTHU,P RTF
      *NTFLG) RTF
C  NDFLAG FLAG TO INDICATE WHICH PASS RTF
C  =0 FIRST PASS RTF
C  =1 SUBSEQUENT PASSES RTF
C  NOTE - THIS ROUTINE REQUIRES INITIALIZATION . RTF
C          ON FIRST PASS, ANGLE1 MUST = THE INITIAL TAKE OFF ANGLE ON RTF
C          GROUND, ANGLE2 MUST =0, RANG12 MUST = RADIUS OF EARTH RTF
C  FREQ-OPERATING FREQUENCY IN MHZ. RTF
C  ANGLE1 - ANGLE (DEG) BETWEEN TILTED LAYER AND RAY INCIDENT ON THE LAY RTF
C  ANGLE2 - TILT ANGLE (DEG) - THAT IS, ANGLE BETWEEN TILTED LAYER AND A RTF
C          EXACTLY HORIZONTAL LAYER AT THE REFLECTION POINT RTF
C  RANG12 - DISTANCE FROM CENTER OF EARTH (KM) OF REFLECTION POINT USED RTF
C          COMPUTE ANGLE1+2 RTF
C  RTU-COMPUTED DISTANCE FROM CENTER OF EARTH IN KM. OF POINT OF INTERES RTF
C  RMU-DISTANCE FROM CENTER OF EARTH TO LAYER IN KM. RTF
C  PNTFLG-PENETRATION FLAG RTF
C          =0. REFLECTION RTF
C          =1. PENETRATION RTF
      IMPLICIT DOUBLE PRECISION (A-H,O-Z) RTF
      DOUBLE PRECISION M3000 RTF
      DIMENSION RM(3),H(3),FC(3),RTH(3) RTF
      COMMON/RIIPAR/M3000,FCF2,FCF1,FCE,HBE,HAE,HME,HAF1,HMF1,HAF2,HMF2, RTF
      IDUM(13),ID(3) RTF
      COMMON/RTCOM/COSB0,NUSE RTF
      DATA RAD/0.1745329251994330D-01/ RTF
      DACOS((DUMMY)=DATAN2(DSQRT(1.000-DUMMY*DUMMY)),DUMMY) RTF
      PNTFLG=0.000 RTF
      IF(NDFLAG)4,4,44 RTF
4      IF(ANGLE2.EQ.0.000)GO TO 44 RTF
      WRITE(5,100) ANGLE2 RTF
100  FORMAT(22H THE VALUE OF ANGLE2 =,D15.8,13H IS IN ERROR.) RTF
      PNTFLG=1.000 RTF
44      FCF(1)=FCE RTF
      FCF(2)=FCF1 RTF
      FCF(3)=FCF2 RTF
      H(1)=HAE RTF
      H(2)=HAF1 RTF
      H(3)=HAF2 RTF
      RM(3)=6370.00+HMF2 RTF
      RM(2)=RM(3)-H(3) RTF
      RM(1)=RM(2)-H(2) RTF
      IF(NDFLAG.GT.0) GO TO 45 RTF
      COSB0=(DCOS(ANGLE1*RAD)*RANG12/6370.00) RTF
45      DO 10 N=1,3 RTF
C  COMPUTE RTH FOR EACH LAYER RTF
      IF(FC(N).EQ.0.000)GO TO 6 RTF
      FAC=(RM(N)**2)/16.00-(H(N)**2/2.00)*((FREQ/FC(N))**2-1.00) RTF
      IF(FAC)6,5,5 RTF
5      RTH(N)=0.7500*RM(N)+DSQRT(FAC) RTF
      GO TO 10 RTF
6      RTH(N)=RM(3) RTF
10      CONTINUE RTF
C  FIND MAX RTH RTF
      RMM=RTH(3) RTF
      IF(RTH(3).EQ.RM(3))RMM=RM(3)/2.000 RTF
3000 IF(NDFLAG.GT.0) GO TO 14 RTF

```

```

C   IF ALL RTM ARE EQUAL, USE F2 LAYER                                RTF
      IF(RTM(2).NE.RTM(3).OR.RTM(1).NE.RTM(3))GO TO 12                RTF
      NUSE=3                                                            RTF
      RTMUSE=RTM(3)                                                    RTF
      GO TO 14                                                          RTF
C   FIND MINIMUM RTM                                                RTF
12   RTMUSE=RTM(1)                                                    RTF
      NUSE=1                                                            RTF
      DO 13 I=2,3                                                      RTF
      IF(RTMUSE.LT.RTM(I))GO TO 13                                     RTF
      RTMUSE=RTM(I)                                                    RTF
      NUSE=I                                                            RTF
13   CONTINUE                                                         RTF
      IF(NDFLAG.GT.0) GO TO 14                                          RTF
123  ANGLE1=(DACOS(COSB0*6370.00/RANG12))/RAD                         RTF
C   USE PARAMETERS ASSOC. WITH MIN RTM                               RTF
14   RTMUSE=RTM(NUSE)                                                  RTF
      RMUSE=RM(NUSE)                                                    RTF
      HUSE=H(NUSE)                                                      RTF
      FCUSE=FC(NUSE)                                                    RTF
144  CBTM=DACOS(ANGLE1*RAD)*RANG12/RTMUSE                             RTF
      IF(CBTM-1.000)15,15,16                                           RTF
15   BTM=DACOS(CBTM)                                                    RTF
17   X=1.000-(((FREQ/FCUSE)**2)*((DSIN(BTM))**2))                    RTF
      IF(X.GE.0.000)GO TO 20                                           RTF
16   IF(RTMUSE.NE.RM(3))GO TO 18                                       RTF
C   PENETRATION                                                     RTF
185  RTU=RMH                                                            RTF
      PNTFLG=1.000                                                      RTF
      RMU=RM(3)                                                         RTF
      RTMU=RTMUSE                                                       RTF
2000 RETURN                                                            RTF
18   IF(NUSE-3)19,185,185                                             RTF
C   ELIMINATE RTM USED AND FIND NEXT SMALLEST RTM                 RTF
19   NUSE=NUSE+1                                                       RTF
      GO TO 123                                                         RTF
C   REFLECTION                                                       RTF
20   RT=RTMUSE-HUSE*DSQRT(X)                                           RTF
      RMU=RMUSE                                                         RTF
      RTMU=RTMUSE                                                       RTF
      A=RMU-PT                                                         RTF
      B=A/DCOS(ANGLE2*RAD)                                             RTF
      IF(B.GE.HUSE)B=HUSE                                              RTF
      RTU=RMU-B                                                         RTF
      END                                                                RTF

```

ROUTINE DENSE

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```

      SUBROUTINE DENSE(R,THETA,PHI,EN,DNDR,DNDT,DNDP)
C  R-DISTANCE FROM CENTER OF EARTH IN KM.
C  THETA-NORTH LATITUDE IN DEGREES
C  PHI-WEST LONGITUDE IN DEGREES
C  EN-VALUE OF ELECTRON DENSITY AT GIVEN POINT
C  DNDR-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO R
C  DNDT-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO THETA
C  DNDP-PARTIAL DERIVATIVE OF ELEC. DEN. WITH RESPECT TO PHI
      IMPLICIT DOUBLE PRECISION (A-H,O-Z)
      DIMENSION RX(9),RY(9),ALPHA(9),FN(9)
      COMMON/PERT/RIIP,ITIP
      DATA RAD/.0174532925199433D0/
10    RY(1)=R
      RX(1)=THETA*RAD
      ALPHA(1)=PHI*RAD
      NSIG=1
20    CALL DERV(NSIG,FN,RY,RX,ALPHA,DNDR,DNDT,DNDP)
      IF(NSIG.EQ.3) GO TO 30
      DO 25 I=2,5
      CALL RIIP(RY(I),RX(I),ALPHA(I),FN(I))
      GO TO (22,23),ITIP
22    CALL NFROMR(RY(I+4),FN(I+4))
      GO TO 25
23    CALL RIIP(RY(I+4),RX(I+4),ALPHA(I+4),FN(I+4))
25    CONTINUE
      CALL RIIP(RY(1),RX(1),ALPHA(1),FN(1))
      NSIG=2
      GO TO 20
30    EN=FN(1)
      RETURN
      END

```

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## Appendix C

### Block Diagram, Flow Chart, and Program Listing for WIMP Driving Program OBLFACT

Explanation:

#### C1. OBLFACT BLOCK DIAGRAM

This presentation illustrates the communication and iteration network employed to generate the  $M(3000)F_2$  and  $f_o F_2$  gradient correction factors required to match the predicted leading edge to the given oblique ionogram. The function of the various blocks is generally described as follows:

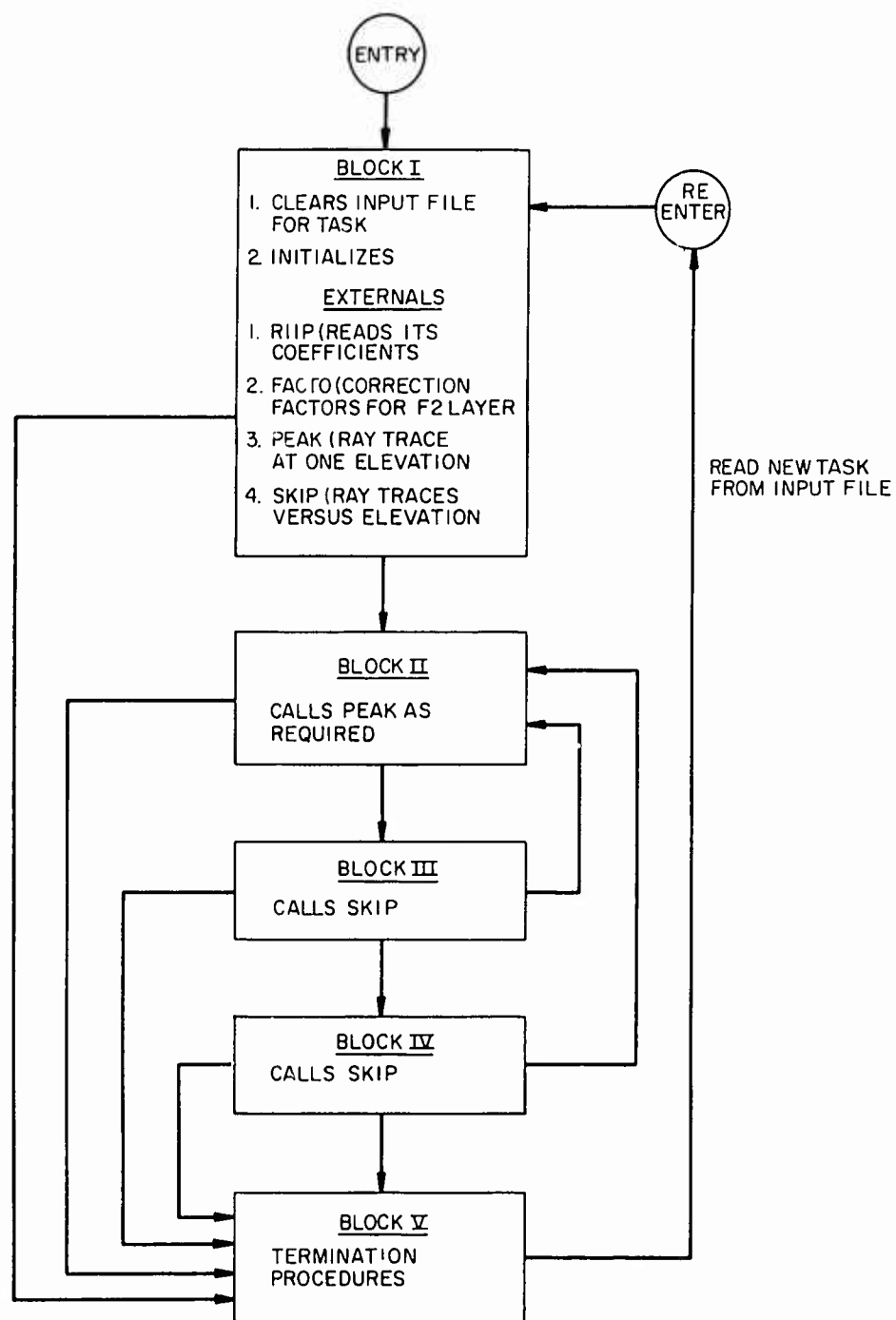
- BLOCK I: Initialization and Input Procedures.
- BLOCK II: Refinement of  $M(3000)F_2$  Gradient Correction Factor.
- BLOCKS III and IV: Refinement of  $f_o F_2$  Gradient Correction Factor.
- BLOCK V: Termination and Output Procedures.

#### C2. DETAILED FLOW CHARTS

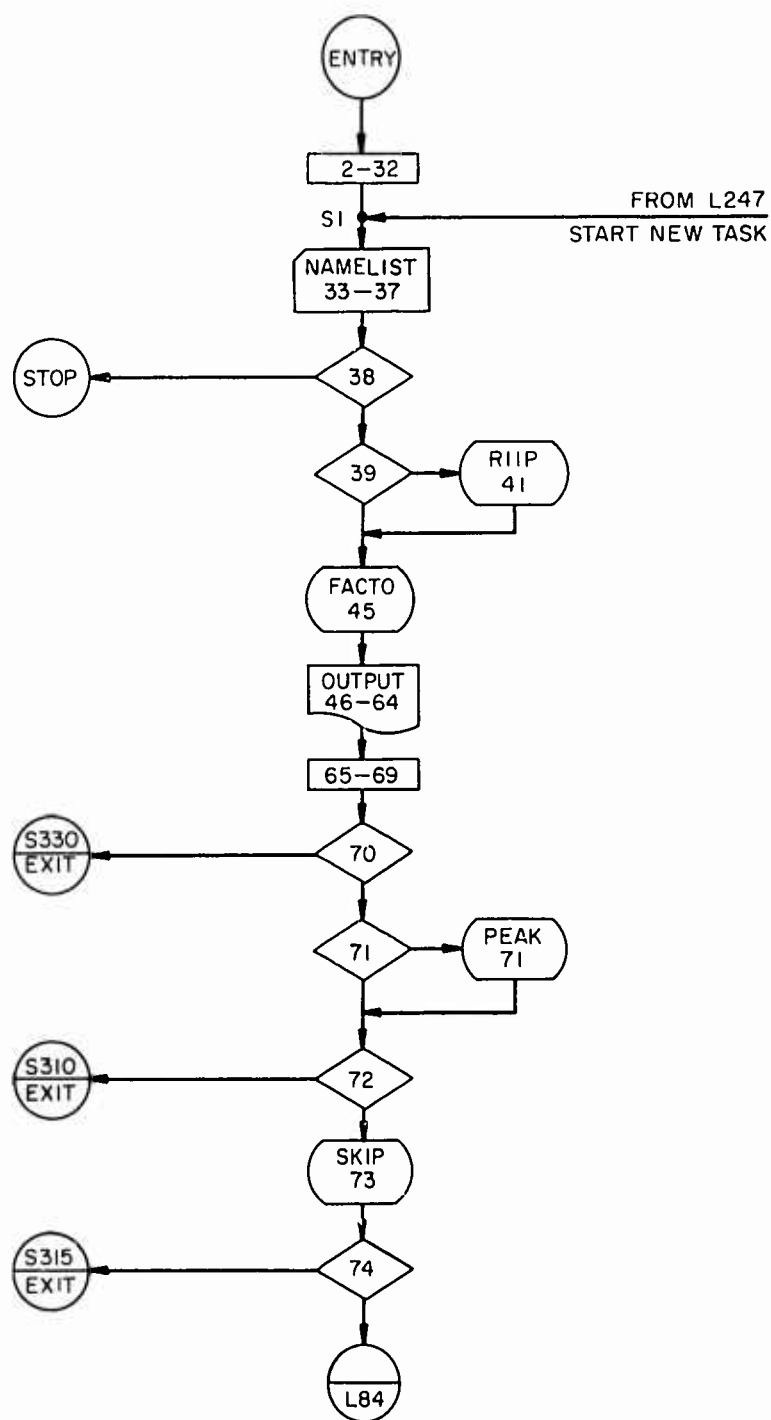
Detailed flow charts are presented for each block. Symbols and conventions are the same as described in Appendix A.

#### C3. PROGRAM LISTING

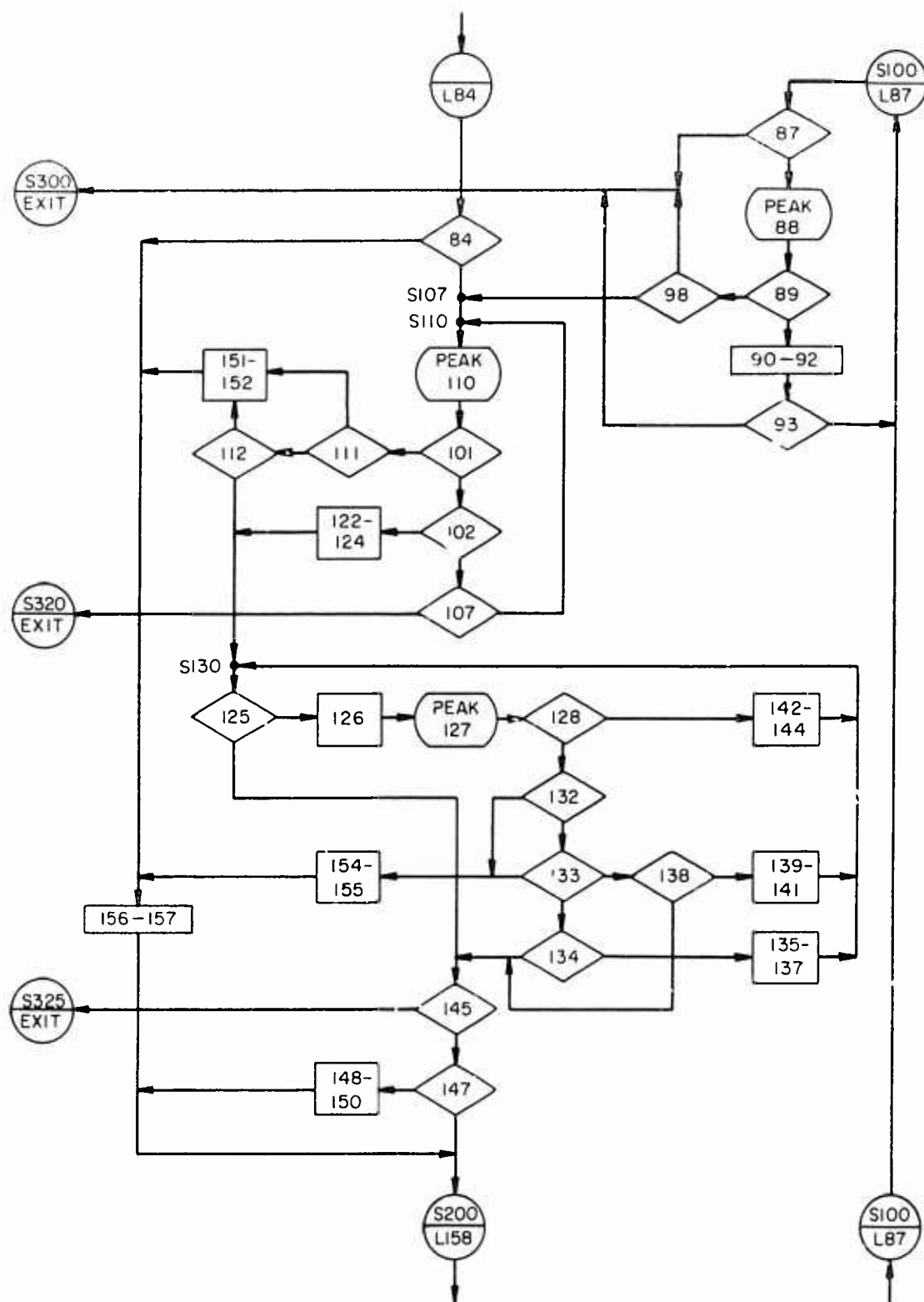
Listings are included for OBLFACT, PEAK, and SKIP.



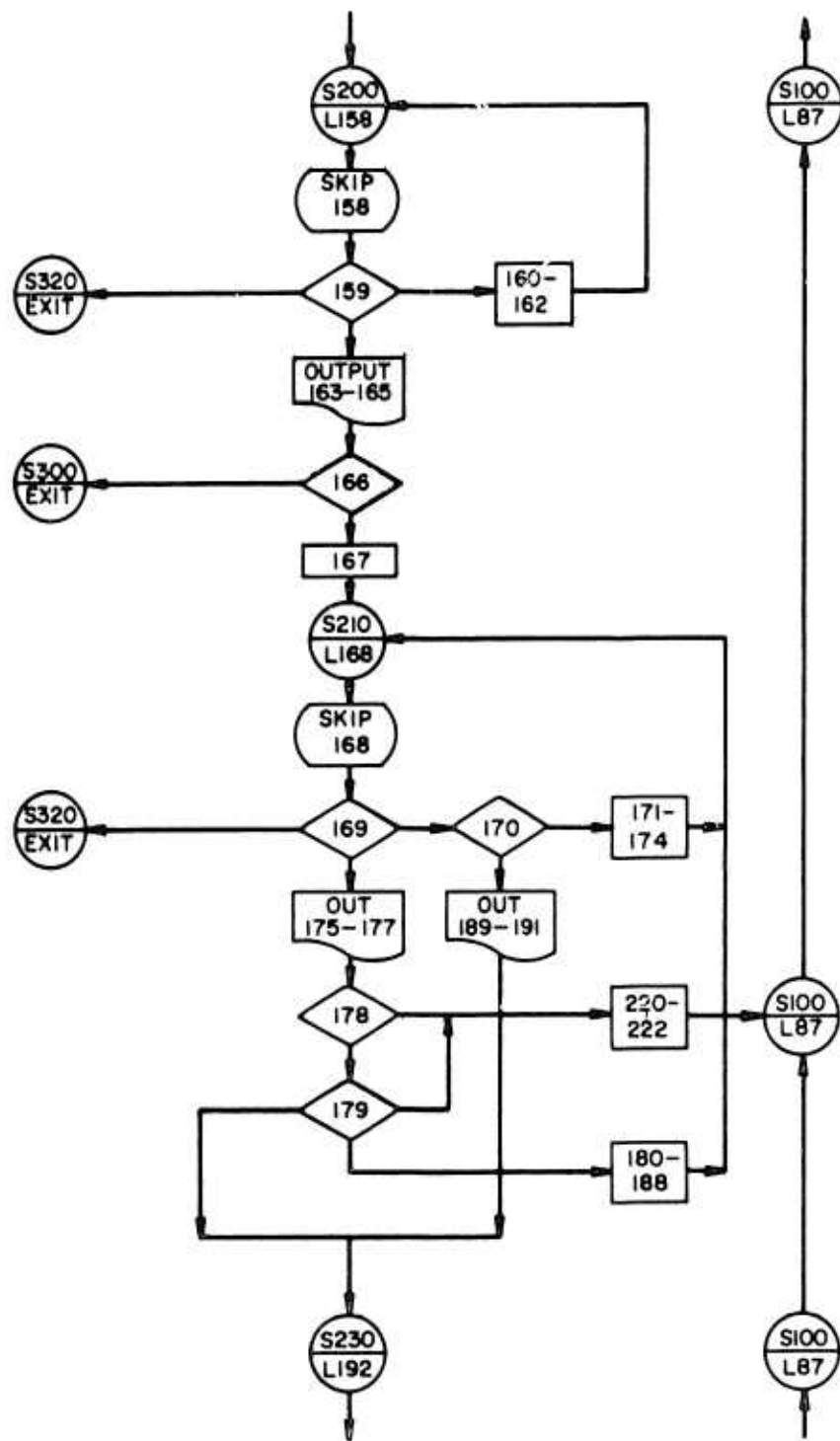
OBLFACT Block Diagram



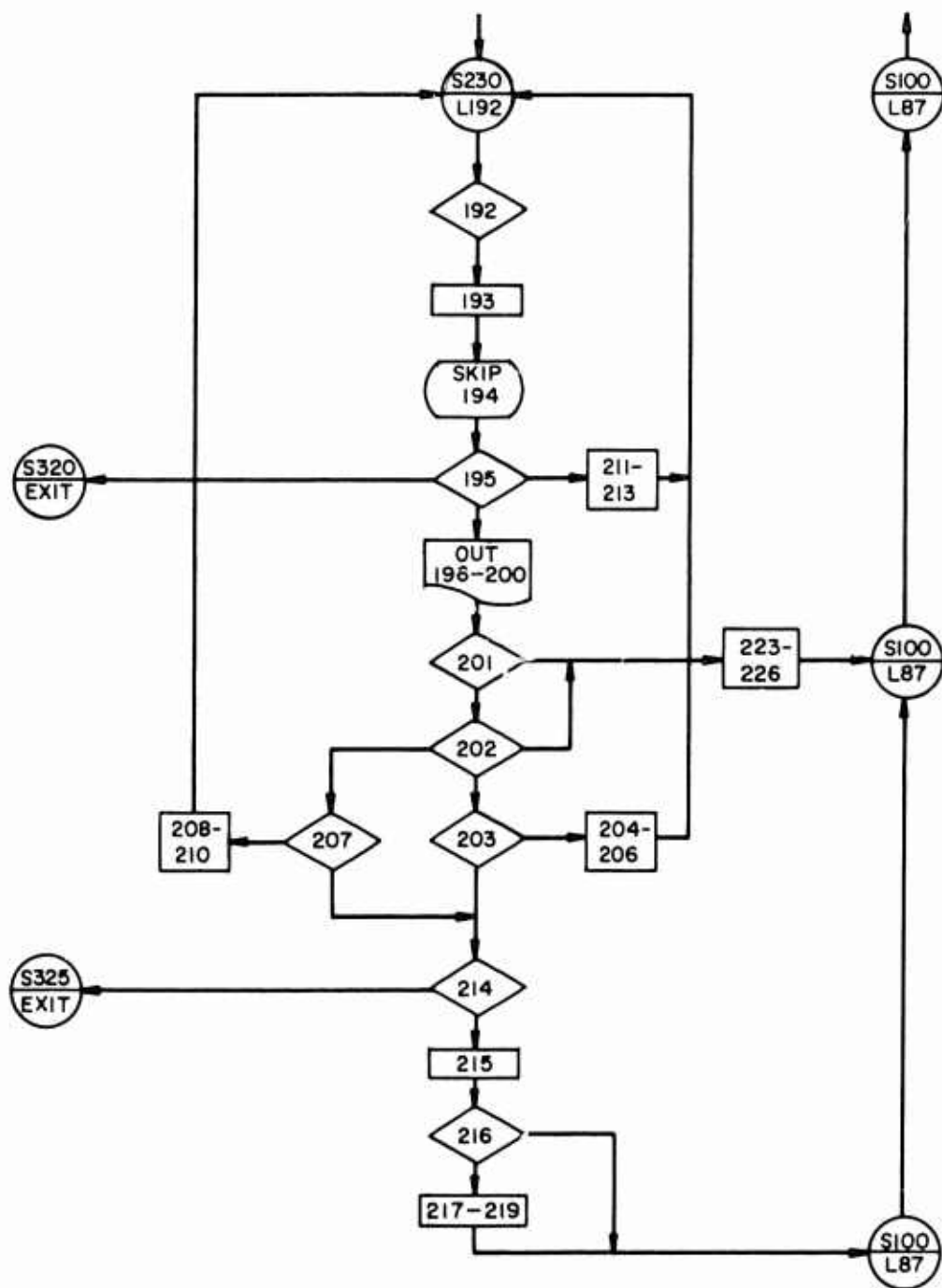
Block I, Detailed Flowchart



Block II, Detailed Flowchart



Block III, Detailed Flowchart



Block IV, Detailed Flowchart

```

SUBROUTINE OBL
C  PROGRAM OBLFACT(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
  IMPLICIT DOUBLE PRECISION(A-H,M,O-Z)
  INTEGER MODE
  DOUBLE PRECISION NL1,NLREF
  LOGICAL SMOOTH,GPNLY
  COMMON/GPFLAG/GPNLY,IWRITE
  COMMON/FIDDLE/FP,FS,R1,NL1,WL1,AZ,RS,ELSTEP,MODE,NSKPCL
  COMMON/PERTC/NLREF,WLREF,PERTP(14)
  COMMON/RIIPAR/DUM1(11),SN,ZT,YRMO,DOY,HAESSET,MFAC,F2FAC,F1FAC,
1  EFAC,H2FAC,DUM2(3),ID,IA,SMOOTH
  NAMELIST/INPUT/SN,ZT,YRMO,DOY,MFAC,F2FAC,
  1NL1,WL1,R1,NLREF,WLREF,RS,AZ,ELSTEP,MODE,
  1FCF2R,HMINR,OCHK,FP,DELP,FS,DELS,MRO,FRO
  3,IRSTRT,ZTREF
  IRSTRT=1
  GPNLY=.TRUE.
  IWRITE=0
  ID=1
  IA=0
  R1=6370.D0
  RS=6370.D0
  MODE=-1
  NL1=
  WL1=
  OCHK=10.D0
  SN30=0.D0
  NLREF=NL1
  WLREF=WL1
  AZ=
  ELSTEP=1.D0
1  FRO=0.D0
  MRO=0.D0
  FP= 0.D0
  DELP=0.D0
  READ(5,INPUT)
  IF(IRSTRT.EQ.0) STOP
  IF(SN30.EQ.YRMO) GO TO 4
  SN30=YRMO
  CALL RIIP(0.D0,0.D0,0.D0,0.D0)
4  IPKNT=0
  FCF2R=- DABS(FCF2R)
  HMINR=- DABS(HMINR)
  CALL FACTO(NLREF,WLREF,FCF2R,HMINR,ZTREF)
CCCC WRITE(6,INPUT)
  WRITE(6,900)SN,ZT,YRMO,DOY,MFAC,F2FAC
900  FORMAT(1X,(SN      =[ ,11X,D24.18/1X,(ZT      =[ ,11X,D24.18/
  *      1X,(YRMO      =[ ,11X,D24.18/1X,(DOY      =[ ,11X,D24.18/
  *      1X,(MFAC      =[ ,11X,D24.18/1X,(F2FAC      =[ ,11X,D24.18)
  WRITE(6,901)NL1,WL1,R1,NLREF,WLREF,RS
901  FORMAT(1X,(NL1      =[ ,11X,D24.18/1X,(WL1      =[ ,11X,D24.18/
  *      1X,(R1        =[ ,11X,D24.18/1X,(NLREF      =[ ,11X,D24.18/
  *      1X,(WLREF      =[ ,11X,D24.18/1X,(RS        =[ ,11X,D24.18)
  WRITE(6,902)AZ,ELSTEP,MODE,FCF2R,HMINR,OCKH
902  FORMAT(1X,(AZ      =[ ,11X,D24.18/1X,(ELSTEP      =[ ,11X,D24.18/
  *      1X,(MODE      =[ ,16X,I3      /1X,(FCF2R      =[ ,11X,D24.18/
  *      1X,(HMINR      =[ ,11X,D24.18/1X,(OCKH      =[ ,11X,D24.18)

```

```

      WRITE(6,903)FP,DELP, FS,DELS, MR0,FR0
903  FORMAT(1X,(FP      =[,11X,024.18/1X,(DELP    =[,11X,024.18/
      *      1X,(FS      =[,11X,024.18/1X,(DELS    =[,11X,024.18/
      *      1X,(MR0     =[,11X,024.18/1X,(FR0     =[,11X,024.18)
      WRITE(6,904)IRSTRT,ZTREF
904  FORMAT(1X,(IRSTRT =[,16X,I3      /1X,(ZTREF  =[,11X,024.18)
      IM01=0
      IF01=0
      NSKPCL=0
      IGOBAK=0
      GPP0=0.00
      IF(DABS(DELP).LT.DCHK.AND.DABS(DELS).LT.DCHK) GO TO 330
      IF(FP.GE.5.7400) CALL PEAK(FR0,MR0,GPP0,IGOBAK)
      IF(IGOBAK.GT.0) GO TO 310
      CALL SKIP(FR0,MR0,GPS0,0,IGOBAK)
      IF(IGOBAK.GT.0) GO TO 315
      GPPDES=GPP0+DELP
      GPSDES=GPS0+DELS
      WRITE(6,111) GPPDES,GPSDES
111  FORMAT(1 DESIRED GPP=[,4P015.2,[, GPS=[,015.2)
      DELP1=DELP
      DELS1=DELS
      DELP0=DELP
      DELS0=DELS
      MR1=MR0
      IF(DABS(DELP).LT.DCHK) GO TO 197
      GO TO 107
C MR FIDDLING
100  IF(FP.LT.5.7400) GO TO 300
      CALL PEAK(FR0,MR0,GPP0,IGOBAK)
      IF(IGOBAK.EQ.0) GO TO 105
      MR1=MR0
      MR0=MR1+.00100
      IPKCNT=IPKCNT+1
      IF(IPKCNT-100) 100,320,320
105  DELP0=GPPDES-GPP0
      NSTMT=105
      WRITE(6,1111) NSTMT,FR0,MR0,DELP0
1111 FORMAT(1I0,1P3015.7)
      IF(DABS(DELP0).LT.DCHK) GO TO 300
107  MR1=MR0-DSIGN(.00100,DELP0)
110  CALL PEAK(FR0,MR1,GPP1,IGOBAK)
      IF(IGOBAK.EQ.0) GO TO 115
      IF(DELP0.GT.0.00) GO TO 128
      MR0=MR1
      MR1=MR0-DSIGN(.00100,DELP0)
      DELP0=-10000.00
      IPKCNT=IPKCNT+1
      IF(IPKCNT-100) 110,320,320
115  DELP1=GPPDES-GPP1
      NSTMT=115
      WRITE(6,1111) NSTMT,FR0,MR1,DELP1
      IF(DABS(DELP1).LT.DCHK) GO TO 190
      IF(DELP1*DELP0) 130,190,120
120  MRR=DELP1*(MR1-MR0)/(DELP0-DELP1)
      IF(DABS(MRR).GT.0.100) MRR=DSIGN(0.100,MRR)
      MRR=MR1+MRR

```



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	IF(-DELP0.EQ.10000.D00.OR.(MR1-MRR)*DELP0.LE.0.000)	
1	MRR=MR1-DSIGN(.00100,DELP1)	
	MR0=MR1	
	MR1=MRR	
	DELP0=DELP1	
	GO TO 110	
128	DELP1=-10000.D0	
	NSTMT=128	
	WRITE(6,1111) NSTMT,FR0,MR1,DELP1	
130	IF(DABS(MR1-MR0).LT..000100) GO TO 180	
	MRR=(MR1+MR0)*.500	
	CALL PEAK(FR0,MRR,GPPR,IGOBAK)	
	IF(IGOBAK.GT.0) GO TO 160	
	DELPR=GPPDES-GPPR	
	NSTMT=130	
	WRITE(6,1111) NSTMT,FR0,MRR,DELPR	
	IF(DABS(DELPR).LT.0CHK) GO TO 195	
	IF(DELPR*DELP0) 150,195,140	
140	IF(DABS(DELPR).GT.DABS(DELP0)) GO TO 180	
	DELP0=DELPR	
	MR0=MRR	
	GOTO 130	
150	IF(DABS(DELPR).GT.DABS(DELP1)) GO TO 180	
	DELP1=DELPR	
	MR1=MRR	
	GOTO 130	
160	DELP1=-10000.D0	
	MR1=MRR	
	GO TO 130	
180	IF(IM01*IF01.EQ.1) GOTO 325	
	IM01=1	
	IF(DABS(DELP1).GE.DABS(DELP0)) GO TO 200	
	DELP0=DELP1	
	MR0=MR1	
	GOTO 200	
190	MR0=MR1	
	DELP0=DELP1	
	GOTO 197	
195	MR0=MRR	
	DELP0=DELPR	
197	IM01=0	
C	FR FIDDLE	
200	CALL SKIP(FR0,MR0,GPS0,1,IGOBAK)	
	IF(IGOBAK-1) 205,201,320	
201	FR1=FR0	
	FR0=FR1+.00100	
	GO TO 200	
205	DELS0=GPPDES-GPS0	
	NSTMT=205	
	WRITE(6,1111) NSTMT,FR0,MR0,DELS0	
	IF(DABS(DELS0).LT.0CHK) GO TO 300	
	FR1=FR0-DSIGN(.00100,DELS0)	
210	CALL SKIP(FR1,MR0,GPS1,1,IGOBAK)	
	IF(IGOBAK-1) 215,211,320	
211	IF(DELS0.GT.0.00) GO TO 228	
	FR0=FR1	
	FR1=FR0-DSIGN(.00100,DELS0)	

```

        DELS0=-10000.00                                OBL
        GO TO 210                                        OBL
215     DELS1=GPSDES-GPS1                                OBL
        NSTMT=215                                        OBL
        WRITE(6,1111) NSTMT,FR1,MRO,DELS1              OBL
        IF(DABS(DELS1).LT.DCHK) GO TO 290               OBL
        IF(DELS1*DELS0) 230,290,220                    OBL
220     FRR=DELS1*(FR1-FR0)/(DELS0-DELS1)              OBL
        IF(DABS(FRR).GT.0.1D0) FRR=DSIGN(0.1D0,FRR)     OBL
        FRR=FR1+FRR                                     OBL
        IF(-DELS0.EQ.10000.0D0.OR.(FR1-FRR)*DELS0.LE.0.0D0) OBL
1       FRR=FR1-DSIGN(.001D0,DELS1)                   OBL
        FR0=FR1                                         OBL
        FR1=FRR                                         OBL
        DELS0=DELS1                                     OBL
        GOTO 210                                        OBL
228     DELS1=-10000.00                                OBL
        NSTMT=228                                        OBL
        WRITE(6,1111) NSTMT,FR1,MRO,DELS1              OBL
230     IF(DABS(FR1-FR0).LT..0001D0) GO TO 280          OBL
        FRR=(FR1+FR0)*.5D0                             OBL
        CALL SKIP(FRR,MRO,GPSR,1,IGOBK)                 OBL
        IF(IGOBK-1) 235,260,320                        OBL
235     DELSR=GPSDES-GPSR                                OBL
        NSTMT=235                                        OBL
        WRITE(6,1111) NSTMT,FRR,MRO,DELSR              OBL
        IF(DABS(DELSR).LT.DCHK) GO TO 295              OBL
        IF(DELSR*DELS0) 250,295,240                    OBL
240     IF(DABS(DELSR).GT.DABS(DELS0)) GO TO 280        OBL
        DELS0=DELSR                                     OBL
        FR0=FRR                                         OBL
        GOTO 230                                        OBL
250     IF(DABS(DELSR).GT.DABS(DELS1)) GO TO 280        OBL
        DELS1=DELSR                                     OBL
        FR1=FRR                                         OBL
        GOTO 230                                        OBL
260     DELS1=-10000.00                                OBL
        FR1=FRR                                         OBL
        GO TO 230                                        OBL
280     IF(IM01*IF01.EQ.1) GO TO 325                    OBL
        IF01=1                                           OBL
        IF(DABS(DELS1).GE.DABS(DELS0)) GO TO 100       OBL
        DELS0=DELS1                                     OBL
        FR0=FR1                                         OBL
        GOTO 100                                        OBL
290     FR0=FR1                                         OBL
        DELS0=DELS1                                     OBL
        GOTO 297                                        OBL
295     FR0=FRR                                         OBL
        DELS0=DELSR                                     OBL
297     IF01=0                                           OBL
        GOTO 100                                        OBL
300     WRITE(6,305) MRO,FR0,DELP0,DELS0              OBL
305     FORMAT(10 CONVERGENT VALUES\ MR=[,1PD15.7,[, FR=[,D15.7/ OBL
        1 10X,[ MISS DIST.  PEAK=[,D10.3,[, SKIP=[,D10.3) OBL

```

ROUTINE OBL

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GOTO 1	OBL
310 WRITE(6,312)	OBL
312 FORMAT((0 PEAK RAYTRACE FAILS ON INPUT CASE, TRY DIFFERENT INPUT())	OBL
GOTO 1	OBL
315 WRITE(6,317)	OBL
317 FORMAT((0 SKIP RAYTRACES FAIL ON INPUT CASE, TRY DIFFERENT INPUT())	OBL
GOTO 1	OBL
320 WRITE(6,322)	OBL
322 FORMAT((0 100 ITERATIONS DONE BUT DOESN'T CONVERGE, [	OBL
1[ TRY DIFFERENT INPUT())	OBL
GOTO 300	OBL
325 WRITE(6,327)	OBL
327 FORMAT((0 CONVERGENCE PROBLEMS, TRY DIFFERENT INPUT())	OBL
GOTO 300	OBL
330 WRITE(6,332)	OBL
332 FORMAT([ YOUR ORIGINAL INPUT CONVERGES])	OBL
GOTO 1	OBL
END	OBL

```

SUBROUTINE SKIP(FRR,MRR,GPS,IOP,IGOBK)
IMPLICIT DOUBLE PRECISION (A-H,O-Z)
REAL OUT(3)
DOUBLE PRECISION MRR,MR,NL1,NLT,NLREF,GP(42),RS2(42)
COMMON/PERTC/NLREF,WLREF,FR,FD,MR,DUM(11)
COMMON/FIDDLE/FP,FS,R1,NL1,WL1,AZ,RS,ELSTEP,MODE,NSKPCL
COMMON/REMWEN/INUSE,NNUSE(20),FCREF(20)
NSKPCL=NSKPCL+1
IF(NSKPCL.GT.100) GO TO 120
IGOBK=0
NELM=20.00/ELSTEP+1.00
FR=FRR
MR=MRR
DO 10 IEL=1,NELM
EL=(IEL-1)*ELSTEP
CALL TRISL(R1,NL1,WL1,AZ,EL,0.00,FS,MODE,RS,RS2(IEL),NLT,HLT,
1PP,GP(IEL),AZF,ELF,SRANGE,ELSR,DIST,BEAR,IREFN)
IF(IREFN-1) 6,8,12
6 DO 7 I=1,INUSE
IF(NNUSE(I).NE.3) GO TO 8
7 CONTINUE
GO TO 10
8 RS2(IEL)=1.020
GP(IEL)=1.020
10 CONTINUE
IEL=NELM+1
12 IF(IEL.EQ.1) GO TO 110
RS2(IEL)=1.020
NELM=IEL-1
IMIN=1
IF=0
DO 20 IEL=1,NELM
IF(RS2(IEL).GT.6378.8500) GO TO 20
IF=1
IF(GP(IEL).LT.GP(IMIN)) IMIN=IEL
20 CONTINUE
IF(IF.EQ.0) GO TO 110
GPS=GP(IMIN)
IF(IOP.EQ.0) GO TO 130
IF(RS2(IMIN+1).LT.6378.8500) GO TO 130
IF(RS2(IMIN+1).GE.0.9020) GO TO 130
IF(GP(IMIN+1).GT.GP(IMIN)) GO TO 130
GPS=GP(IMIN)+(GP(IMIN+1)-GP(IMIN))*(6378.8500-RS2(IMIN))/
1 (RS2(IMIN+1)-RS2(IMIN))
GO TO 130
110 IGOBK=1
GO TO 130
120 IGOBK=2
130 OUT(1)=FR
OUT(2)=MR
OUT(3)=GPS
WRITE(6-140) OUT,IGOBK
140 FORMAT(1 SKIP(,2F10.6,F10.2,I5)
RETURN
END

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74/74      OPT=1

FTN 4.5+414

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SUBROUTINE PEAK(FRR,MRR,GPP,IGOBAK)
IMPLICIT DOUBLE PRECISION(A-H,O-Z)
REAL OUT(3)
DOUBLE PRECISION MRR,NL1,NLT,ELP(25),NLREF,MR
COMMON/PERTC/NLREF,MLREF,FR,FD,MR,DUM(11)
COMMON/FIDDLE/FP,FS,R1,NL1,HL1,AZ,RS,ELSTEP,MODE,NSKPCL
COMMON/REMWEN/INUSE,NNUSE(20),FCREF(20)
DATA ELP/11.900,10.300,8.900,7.700,6.700,5.900,5.200,4.600,
1 4.100,3.900,5.200,4.800,4.500,4.200,4.00,3.800,2*3.700,
2 2*3.600,3*3.500,2*3.400/
FR=FRR
MR=MRR
IF=FP-4.7400
CALL TRISL(R1,NL1,HL1,AZ,ELP(IF),0.00,FP,MODE,RS,
1RS2,NLT,NLT,PP,GPP,AZF,ELF,SRANGE,ELSR,DIST,BEAR,IGOBAK)
IF(RS2.GT.6378.8500) IGOBAK=1
DO 1 I=1,INUSE
IF(NNUSE(I).NE.3) IGOBAK=1
1 CONTINUE
OUT(1)=FR
OUT(2)=MR
OUT(3)=GPP
WRITE(6,11) OUT,IGOBAK
11 FORMAT(1X,PEAK(,2F10.6,F10.2,I5)
RETURN
END

```